



Vibration Monitoring Assessment Report | August 2023

Tweed Valley Hospital 771 Cudgen Road, Cudgen NSW

Prepared for: Lendlease Building Pty Ltd

Job Number: A101021.0286.00 VIB49 v1f | Date: 11/09/2023



ADE
CONSULTING
GROUP

Document Information



Report Title: Vibration Monitoring Assessment Report | August 2023
 Prepared for: Lendlease Building Pty Ltd
 Project Address: Tweed Valley Hospital 771 Cudgen Road, Cudgen NSW
 Report Reference: A101021.0286.00 VIB49 v0.1d
 Date: 15/08/2023

Document Control

| Version | Date | Author | Revision description | Reviewer |
|---------|------------|-----------------|-----------------------------|-----------|
| V0.1d | 5/09/2023 | David S O'Brien | Draft for internal review | M McAuley |
| V1F | 18/08/2023 | David S O'Brien | Issue | |
| V1.1F | 8/11/2023 | S. Clouston | Re-release of V1F to client | |

For and on behalf of

ADE Consulting Group Pty Ltd

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Executive Summary

ADE Consulting Group Pty Ltd (ADE) was commissioned by Lendlease Group (Lendlease) to assess the levels of construction related vibration during the construction of the Tweed Valley Hospital Project and associated road works, located at 771 Cudgen Road, Cudgen NSW.

This report summarises vibration data collected at three (3) locations during the monitoring period of July 2023, each device is positioned along the south and southwest of Cudgen Road. At the time of preparing this report and the monitoring period which it covers (July 2023), CD Civil are on site completing planned road work activities on Cudgen Road, and Lendlease are completing superstructure works and trade fitouts of the primary hospital premises. Works anticipated for completion in July and August include landscaping and traffic signal installation works.

The road works and associated auxiliary construction activities that are underway are in close proximity to the vibration loggers, each of which is positioned in close proximity to, or at representative locations relative to, residential receivers.

This report summarises July results as follows:

- Velocity
 - No impact of concern
- Acceleration and Vibration Dose Values
 - No impact of concern.

Contents

| | | |
|----------|--|------------|
| 1 | Introduction | 1 |
| 1.1 | Introduction | 1 |
| 1.2 | Project background | 1 |
| 1.2.1 | Development consent SSD-10353 | 2 |
| 1.2.2 | Monitoring Locations | 3 |
| 2 | Vibration guidelines summary | 4 |
| 2.1 | Guideline vibration values | 4 |
| 2.1.1 | Structural/Cosmetic damage | 4 |
| 2.1.2 | Safe working distances | 7 |
| 2.1.3 | Human comfort | 8 |
| 3 | Results overview | 10 |
| 3.1 | Survey instrumentation and methodology | 10 |
| 3.2 | Results | 10 |
| 3.2.1 | Velocity | 10 |
| 3.2.2 | Acceleration/VDV | 14 |
| 3.3 | Discussion | 16 |
| 4 | Conclusion | 17 |
| | Appendix I – Glossary | i |
| | Appendix II – Aerial Photograph | iii |
| | Appendix III – References | v |
| | Appendix IV – Site Photographs | vi |

1 Introduction

1.1 Introduction

ADE Consulting Group Pty Ltd (ADE) was engaged by the Lendlease Group (Lendlease) to assess the levels of construction related vibration during the construction of the Tweed Valley Hospital Project and associated road upgrades located at 771 Cudgen Road, Cudgen in New South Wales (hereinafter referred to as ‘the Site’).

At the time of vibration monitoring, Lendlease was continuing superstructure works on the Site which includes the construction of columns and suspended slabs. CD Civil was undertaking roadworks associated with the development on Cudgen Road which includes construction of an intersection to the new hospital development, construction of permanent footpaths, stormwater drainage construction (trenching works), road pavement and widening. Works anticipated for completion in July and August include landscaping and traffic signal installation works.

The road improvement works includes the use of large 10T vibratory rollers, multi-tyred rollers, generators, excavators, graders and asphalt machines.

The purpose of environmental monitoring is to:

- Assess construction related ground borne vibration levels against regulatory requirements, development consent conditions, Australian guidelines, and international standards for construction vibration management and control on construction sites
- Manage and mitigate potentially excessive vibration generation through site planning and the adoption of appropriate work methods and practices where feasible and reasonable
- Monitor and assess construction impacts likely to cause adverse comment by the community or impact surrounding sensitive receivers/structures, and provide feasible and reasonable recommendations to manage the impacts
- Establish and maintain positive relationships with project stakeholders.

The purpose of the Vibration Monitoring Assessment (VMA) report is to assess the potential impacts arising from construction activities associated with the Tweed Valley Hospital Project have had on vibration levels on site and comply with the Tweed Valley Hospital– Noise and Vibration Management Plan.

In line with the conditions **C18 – C20** and **B16** set out in the development consent (summarised below in Section **1.2.1**) as well as the relevant goals in **Section 2** the primary aim is to minimise the identified vibration impacts and preserve the public amenity of the local area during construction in accordance with the Development Consent and Guidelines.

This report uses specific terminology. A general vibration and acoustic glossary is provided in **Appendix I – Glossary**.

1.2 Project background

On 13 June 2017, the NSW Government announced an allocation of approximately \$534M for the development of a new hospital on a greenfield site in the Tweed Valley area. The site of the new Tweed Valley Hospital (the Project) is located at 771 Cudgen Road, Cudgen in New South Wales.

An Environmental Impact Statement (EIS) was prepared to accompany a State Significant Development Application for the Project which was assessed under Part 4 of the *Environmental Planning and Assessment Act 1979* (EP&A Act).

An overview of the project specific information is provided in **Table 1** below.

Table 1 Project Specific Information

| Site Details | |
|----------------------------|--|
| Client Name: | Lendlease |
| ADE Project Number: | A101021.0286.00 |
| Site Address: | 771 Cudgen Road, Cudgen NSW (Lot 11 DP 1246853) |
| Date of Report: | 11/09/2023 |
| Development Consent | SSD-10353, Health Administration Corporation. Authorized by the Minister for Planning and Public Spaces on 9 March 2020. Consent approved on 12 June 2020. |
| Objectives: | <ul style="list-style-type: none"> Comply with DIN 4150-3:2016 guidelines and conditions C18 - C20 of Development Consent SSD-10353 Manage potential vibration impacts from construction activities which have the potential to affect the nearby buildings (Kingscliff TAFE and residential properties) To manage the generation of vibration which could affect the neighbours of the Site, workers on the Site, associated buildings, and other members of the public Establish and maintain good relationships with the neighbours and wider community. |
| Key Legislation: | <p>Protection of the Environment Operations Act 1997 (NSW) (POEO Act). The POEO Act is a key piece of environmental protection legislation and regulates activities via:</p> <ul style="list-style-type: none"> Environmental protection licensing, as per schedule 1 Regulation of scheduled and non-scheduled activities Environmental protection offences and penalties Establishment of a <i>general duty of care</i> to notify <i>environment harm</i>. |

1.2.1 Development consent SSD-10353

The consent of approval conditions regarding vibration are summarised below in **Table 2**.

Table 2 Development Consent Conditions

| Condition of Approval number | Detail of Condition Requirement |
|------------------------------|---|
| C18 | <p>Vibration caused by construction at any residences or structure outside the site must be limited to:</p> <ol style="list-style-type: none"> For structural damage, the latest version of DIN 4150-3 (1992-02) Structural Vibration- Effects of vibration on structures (German Institute for Standardisation, 1999) For human exposure, the acceptable vibration values set out in the Environmental Noise Management Assessing Vibration: A Technical Guideline (DEC, 2006) (as may be updated or replaced from time to time) |
| C19 | Vibratory compactors must not be used closer than 30 m from residential buildings unless vibration monitoring confirms compliance with the vibration criteria specified in <i>Condition C18</i> |
| C20 | The limits in conditions C18 and C19 apply unless otherwise outlined in the CNVMSP, approved as part of the CEMP required by <i>Condition of Approval (CoA) B16</i> of this consent |

Note: CoA B16 refers to an approved condition stated in the Lendlease's Construction Noise and Vibration Management Sub-Plan (CNVMSP)

1.2.2 Monitoring Locations

Prior to the commencement of roadworks and in response to the program of works, the vibration monitoring equipment was relocated on 17 November 2022 along the southern alignment of Cudgen Road at three designated locations (ie Monitoring Locations 005, 006 & 007).

The monitoring locations were established to assess the potential vibration impacts to the nearest sensitive receivers and comply with the requirements and conditions set out in the Tweed Valley Hospital– Noise and Vibration Management Plan.

All monitoring locations are within close proximity to the boundary of the nearest sensitive receivers (residential and commercial) that may be impacted by vibration generated from the current roadworks program and associated plant.

Aerial imaging and monitoring location overview is presented in **Appendix II – Aerial Photograph**.

2 Vibration guidelines summary

Vibration criteria and guidelines values for sensitive structures and human comfort are derived from Australian guidelines and International Standards for the purpose of assessment.

2.1 Guideline vibration values

International standards from Germany and the United Kingdom are used in conjunction with the NSW guideline *Assessing Vibration: A Technical Guideline* (DEC, 2006) for assessment of measurement data. The DEC guideline is an informal guideline for assessment of vibration under Australian conditions. The document outlines, summarises, and provides guidance for the assessment of vibration.

The International Standards and the DEC guideline provide best practice assessment for intermittent, transient, and continuous vibration that is commonly generated by construction and roadwork activity.

These standards and guidelines offer guidance for the assessment of:

- Human perception to vibration
- Structures sensitive to vibration
 - Residential buildings
 - Commercial
 - Heritage or other sensitive
 - Buried pipework or other utility services including concrete and masonry.

2.1.1 Structural/Cosmetic damage

For the assessment of the potential for vibration induced structural or cosmetic damage of buildings, the German Standard DIN4150-3:2016 is primarily used when examining the vulnerability of ground-related services and structures to vibration.

The DIN criteria have been adopted for building damage as they are more stringent and, although they vary based on the frequency range of the predominant pulse, can be summarised as 5 mm/s for residential dwellings.

Table 3 below provides guideline values for evaluation of long-term vibration on buildings.

Table 3 Guideline values for evaluating the long-term vibration effects on buildings

| Type of building | Guideline values for $v_{i, \max}$ mm/s (PPV) | |
|---|--|---|
| | Topmost floor, horizontal direction, all frequencies | Floor slab, vertical direction, all frequencies |
| Buildings used for commercial purposes, industrial buildings, and buildings of similar design | 10 | 10 |
| Residential buildings and buildings of similar design and/or occupancy | 5 | 10 |
| Structures that, because of their particular sensitivity to vibration, cannot be classified as above and are of great intrinsic value (e.g. listed buildings) | 3 | 10 |

Note: Bold represents project-specific vibration guidelines

Short term vibration which includes works such as impact pile driving, excavation, and rock breaking which would cause impulsive or intermittent vibration impacts on the surrounding receivers is assessed as transient PPV vibration, guidance is taken from the DIN 4150 standard.

Table 4 below provides guidance for values for Peak Particle Velocity (PPV) at the foundation of the structure and at the plane of the topmost floor. **Table 4** illustrates particle velocity and damage (cosmetic or structural) is frequency dependent (ie that the lower the frequency the more sensitive the structure may be to vibration).

Table 4 Guideline Values for Vibration Velocity (Evaluating Effects of Short-Term Vibration on Structures)

| Line | Type of Structure | Peak Particle Velocity, mm/s | | | | |
|------|---|---------------------------------|-----------------|-----------------|-------------------------------------|---------------------------------|
| | | At foundation at a frequency of | | | Highest floor, horizontal direction | Floor Slabs, vertical direction |
| | | 1 to 10 Hz | 10 to 50 Hz | 50 to 100 Hz | All Frequencies | All Frequencies |
| 1 | Buildings used for commercial purposes, industrial buildings and buildings of similar design | 20 | 20 to 40 | 40 to 50 | 40 | 20 |
| 2 | Dwellings and buildings of similar design and/or occupancy | 5 | 5 to 15 | 15 to 20 | 15 | 20 |
| 3 | Structures that, because of their particular sensitivity to vibration, cannot be classified under lines 1 and 2 and are of great intrinsic value (e.g. listed buildings under preservation order) | 3 | 3 to 8 | 8 to 10 | 8 | 20 |

Note: Bold represents project-specific vibration guidelines

A graphical representation of **Table 4** is shown below in **Figure 1**.

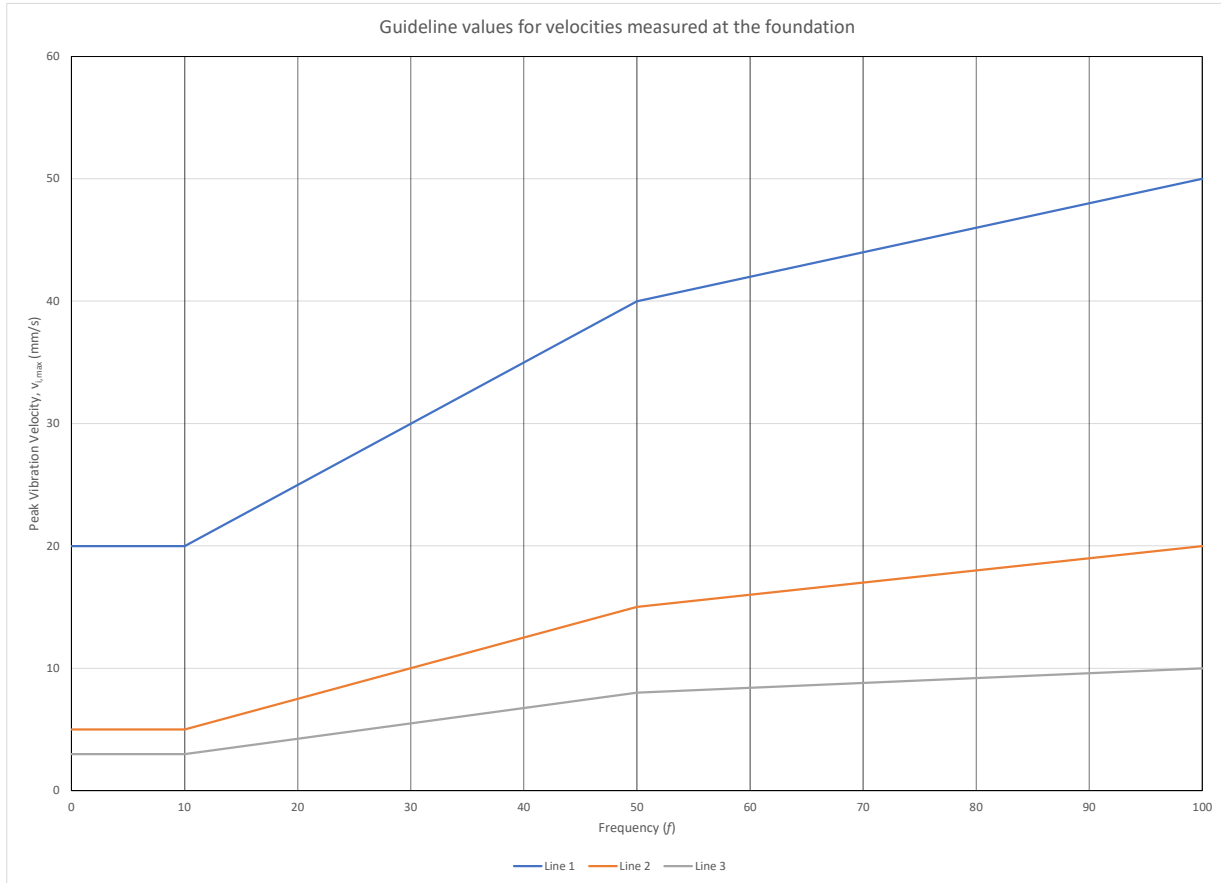


Figure 1 Illustration of the DIN4150 guideline. Structural sensitive to vibration is a function of frequency and velocity

2.1.2 Safe working distances

The Construction Noise and Vibration Strategy (CNVS, TfNSW 2019) outlines the minimum safe working distances for vibration intensive plant for the surrounding vibration sensitive receivers.

As a guide, the minimum working distances for typical vibration intensive plant are listed in **Table 5**. These minimum working distances are summarised for both cosmetic damage (BS 7385 and DIN 4150) and human comfort (*Assessing Vibration: A Technical Guideline*).

Table 5 Recommended minimum working distances from vibration intensive plant (TfNSW CNS)

| Plant Item | Approximate Size / Weight / Model | Minimum Distance for Cosmetic Damage (BS7385) | Minimum Distance for Human Response (DEC Assessing Vibration) | Heritage (DIN4150) |
|-------------------------|-----------------------------------|---|---|--------------------|
| Vibratory Roller | 1-2 tonne | 5 m | 15 – 20 m | 11 m |
| | 2-4 tonne | 6 m | 20 m | 14 m |
| | 4-6 tonne | 12 m | 40 m | 27 m |
| | 7-13 tonne | 15 m | 100 m | 33 m |
| | 13-18 tonne | 20 m | 100 m | 44 m |
| | >18 tonne | 25 m | 100 m | 55 m |
| Small Hydraulic Hammer | 300 kg (5 to 12T excavator) | 2 m | 7 m | 5 m |
| Medium Hydraulic Hammer | 900 kg (12 to 18T excavator) | 7 m | 23 m | 16 m |
| Large Hydraulic Hammer | 1600 kg (18 to 34T excavator) | 22 m | 73 m | 49 m |
| Pile Driver – Vibratory | Sheet piles | 2 to 20 m | 20 m | 15 m ^B |
| Piling Rig - Bored | ≤ 800 mm | 2 m (nominal) | n/a | 6 m ^A |
| Piling Rig – Hammer | 12 T down force | 15 m | 50 m | 45 m ^A |
| Jackhammer | Hand held | 1 m | Avoid contact with structure | 3 m |

Note: Where works occur closest to a sensitive receiver which is designated as a heritage structure, more stringent conditions may apply. For this, a conservative minimum cosmetic damage distance multiplied by 2.2 is used as a guide only

Note A: Data taken from BS5228-2:2009

Note B: Conservative estimate

2.1.3 Human comfort

Construction activities which have the potential to create ground-borne vibrations may impact sensitive receivers near the project works. Humans are responsive to vibration and some discomfort may arise due to various activities, their intensity and duration.

For assessment of human comfort and exposure to vibration, the NSW document *Assessing Vibration: A Technical Guideline* (DEC, 2006) provides direction derived from the British Standard BS6472-1:2008 *Guide to evaluation of human exposure to vibration in buildings. Part 2: Vibration sources other than blasting*.

Table 6 below tabulates the Vibration Dose Values (VDV) for human comfort. These values represent a guideline for the total accumulation of vibration energy during a 15-hour day-time period where the vibration would be experienced. VDV is the total accumulated energy over time.

Table 6 Vibration Dose Values (VDV) for Intermittent Vibration

| Location | Period | Preferred value, VDV m/s ^{1.75} | Maximum value VDV m/s ^{1.75} |
|--|--------------|---|--|
| Critical areas | Day or Night | 0.1 | 0.2 |
| Residences | Day | 0.2 | 0.4 |
| | Night | 0.13 | 0.26 |
| Offices, schools, educational institutions and places of worship | Day or Night | 0.4 | 0.8 |
| Workshops | Day or Night | 0.8 | 1.6 |

Note: Daytime is 07:00 am to 22:00 pm

A 16 hour dosage is used for daytime to assess the dosage of vibration for a whole-day

Note: **Bold** indicates project-specific relevance

Table 7 below tabulates guideline VDV ranges in residential buildings at which a human response or adverse comment to construction vibration would be likely.

These levels are derived from BS6472-2 and provide a subjective judgement for which vibration onsite may result in adverse comment by those who experience it, and to which this monitoring report is assessed against.

Table 7 Vibration Dose Value ranges which might result in various probabilities of adverse comment within residential buildings

| Place and time | Low probability of adverse comment ¹ m/s ^{1.75} | Adverse comment possible m/s ^{1.75} | Adverse comment probable ² m/s ^{1.75} |
|-------------------------------------|--|---|--|
| Residential buildings 16 hr day | 0.2 to 0.4 | 0.4 to 0.8 | 0.8 to 1.6 |
| Residential buildings 8 hr night | 0.1 to 0.2 | 0.2 to 0.4 | 0.4 to 0.8 |

Note 1: Below these ranges adverse comment is not expected

Note 2: Above these ranges adverse comment is likely

Note 3: For offices and workshops, multiplying factors of 2 and 4 respectively should be applied to the above vibration dose ranges for 15h day.

At levels within the ranges tabulated above, the probability for which a comment may be made from the community increases with increased vibration energy from the site.

The degree of the dosage would determine the nature of the vibration perceived which may be experienced by occupants of nearby vibration sensitive receivers.

3 Results overview

3.1 Survey instrumentation and methodology

To assess the potential impacts and ground-borne vibration generated from the current works program, vibration measurements were recorded at three (3) locations in the July 2023 monitoring period utilising Class 1 four-channel Svantek SVAN 958A Sound & Vibration Analysers.

These vibration monitors are enclosed in a weather resistant environmental case which is placed on the ground and covered with a tarp to aid in keeping temperatures below 60°C to prevent and avoid temperature related failures, and moisture intrusion images relating to the installation of the loggers is provided in **Appendix II – Aerial Photograph** and **Appendix IV – Site Photographs**.

The tri-axial accelerometer is placed firmly against the soil surface and covered with a sandbag to minimise external interference. The monitors are positioned external to the Site along the boundary to sensitive receivers adjacent Cudgen Road to the south and southeast.

A summary of the vibration monitoring equipment is provided in **Table 8** below.

Table 8 Vibration equipment deployed

| Make | Model | Location | Serial Number | Calibrated on | Calibration Due |
|---------|-----------|----------|---------------|---------------|-----------------|
| Svantek | SVAN958AG | 005 | 98323 | 12/10/2022 | 12/10/2024 |
| Svantek | SVAN958AG | 006 | 92835 | 18/02/2022 | 18/02/2024 |
| Svantek | SVAN958AG | 007 | 92834 | 9/03/2022 | 9/03/2024 |

3.2 Results

The DIN4150 standard illustrates how lower frequencies have more stringent velocity thresholds for all types of structures, although this is considered a conservative guideline and would vary on a case-by-case basis. For the Tweed Valley Hospital Development, the loggers are positioned, where feasible and reasonable, within reasonable proximity to residential receivers, hence the Line 2 thresholds are adopted for conservative approximation when assessing the vibration on these structures.

Where velocity measurements exceed the Line 2 thresholds, an analysis of the collected data is assessed and a judgement is made as to whether the data is extraneous in nature, or a legitimate construction impact. Where a legitimate impact is noted, ADE liaise with the contractor to discuss the cause of the potential exceedance, and determine if the activity may warrant any concern to any of the structures.

3.2.1 Velocity

A steady decrease in vibration intensive activities have been noted along Cudgen Road. Construction works have concluded, and no vibration intensive activities have been noted.

Figure 2 below presents the velocity (PPV mm/s) at Location L.005 situated by a residential and commercial receiver.

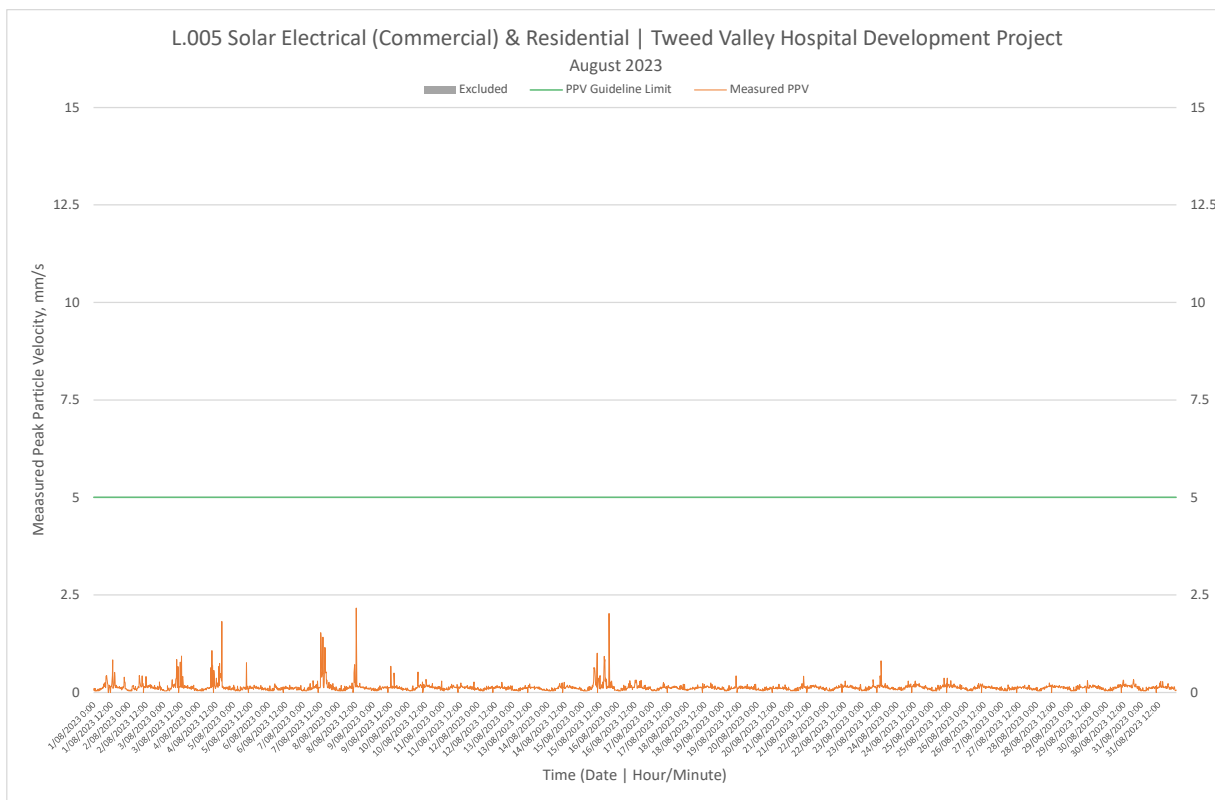


Figure 2 Velocity over time (Logger 005 - Residential/Commercial)

Figure 3 below presents frequency over velocity data for logger L.005.

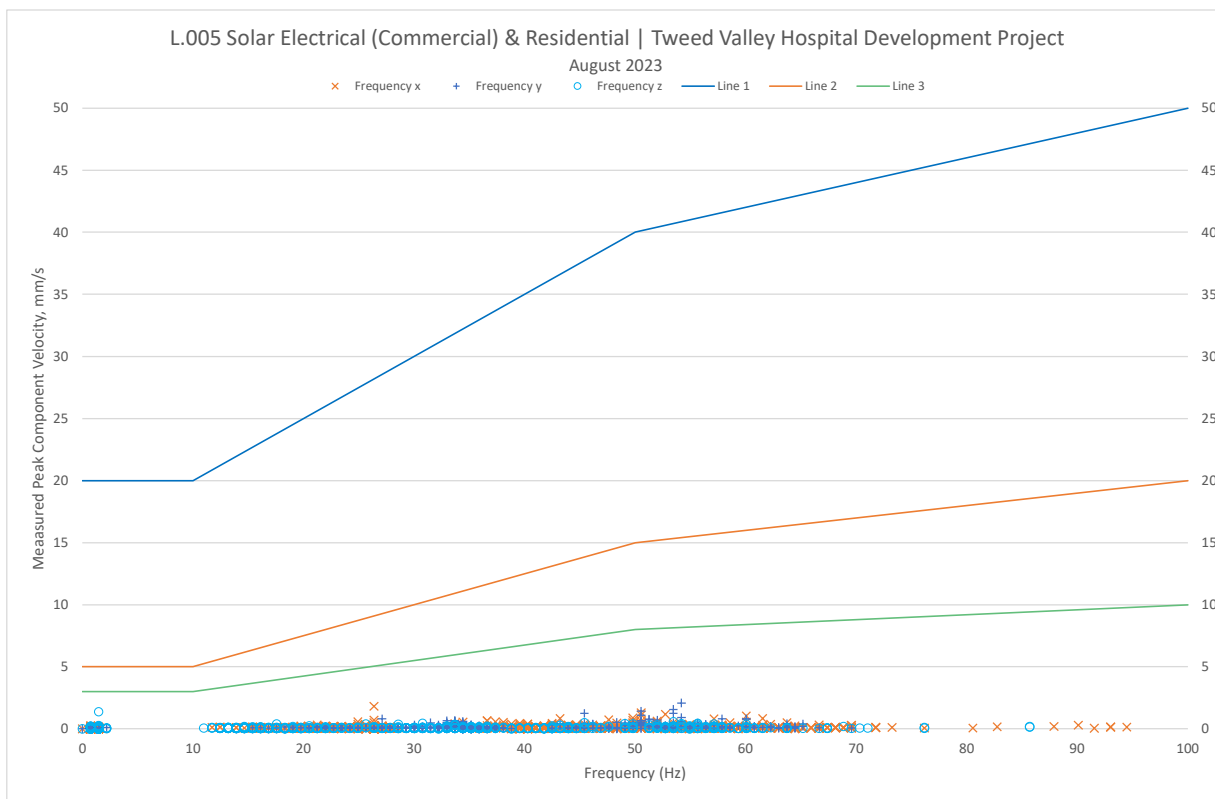


Figure 3 Frequency over Velocity (Logger 005 – Residential/Commercial)

Figure 6 below presents velocity data for the logger located to a commercial and residential premises ('Mate and Matt's') nominated as Location L.006.

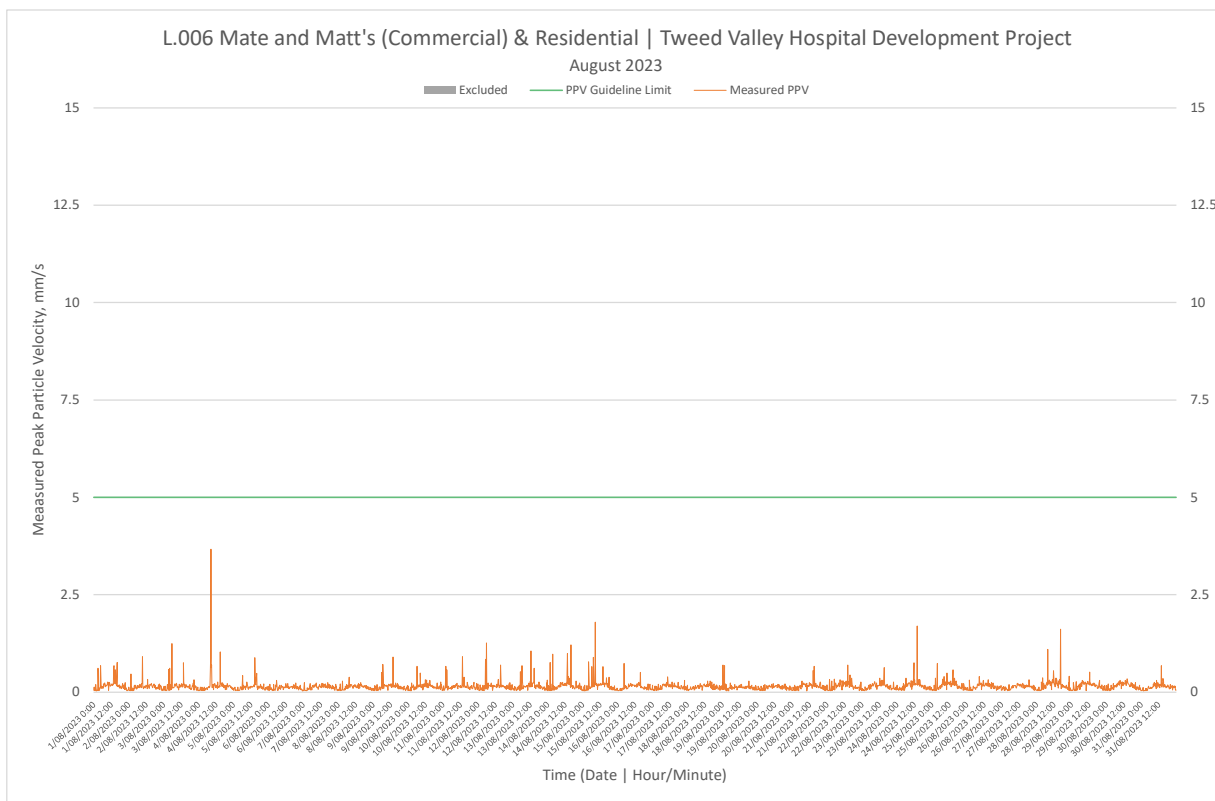


Figure 4 Velocity over time (Logger 006 – Residential/Commercial)

Figure 5 below illustrates the frequency over the velocity for each axis at Location L.006.

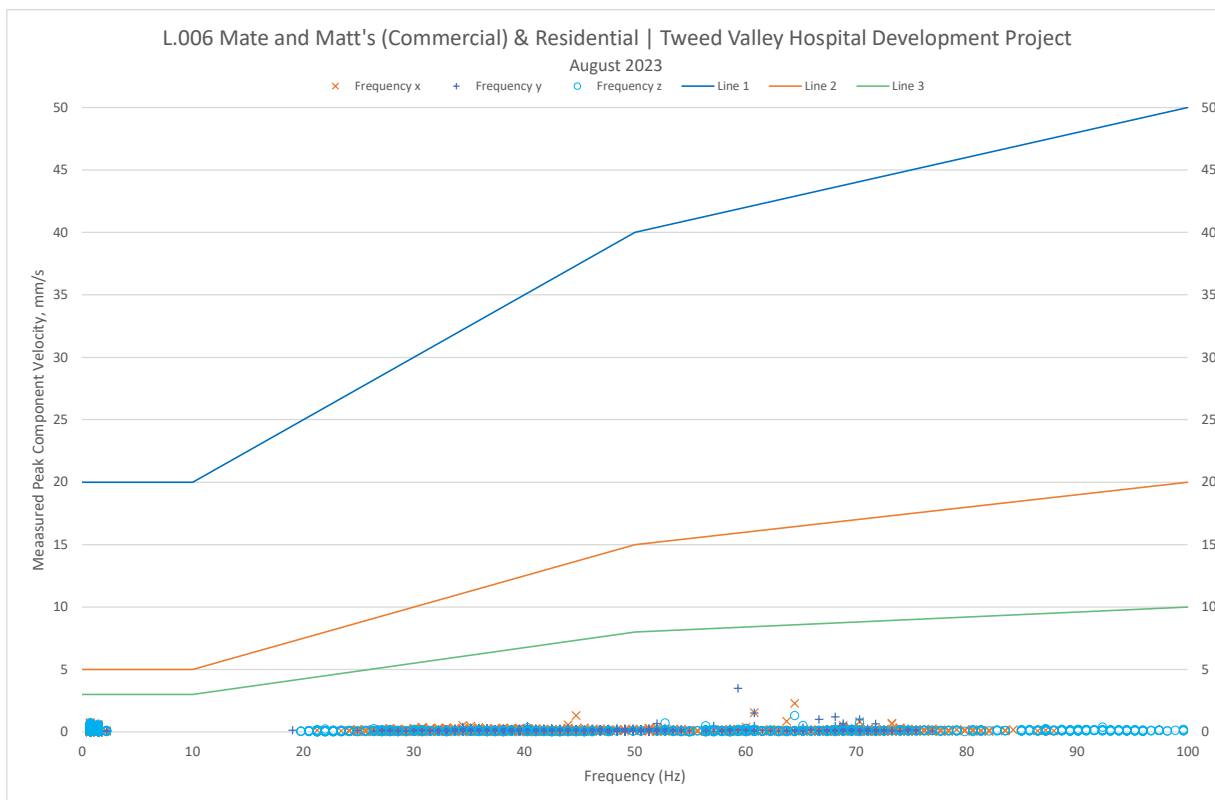


Figure 5 Frequency over Velocity (Logger 006 – Residential/Commercial)

Figure 6 below presents velocity data for logger L.007 located in close proximity to a residential premises.

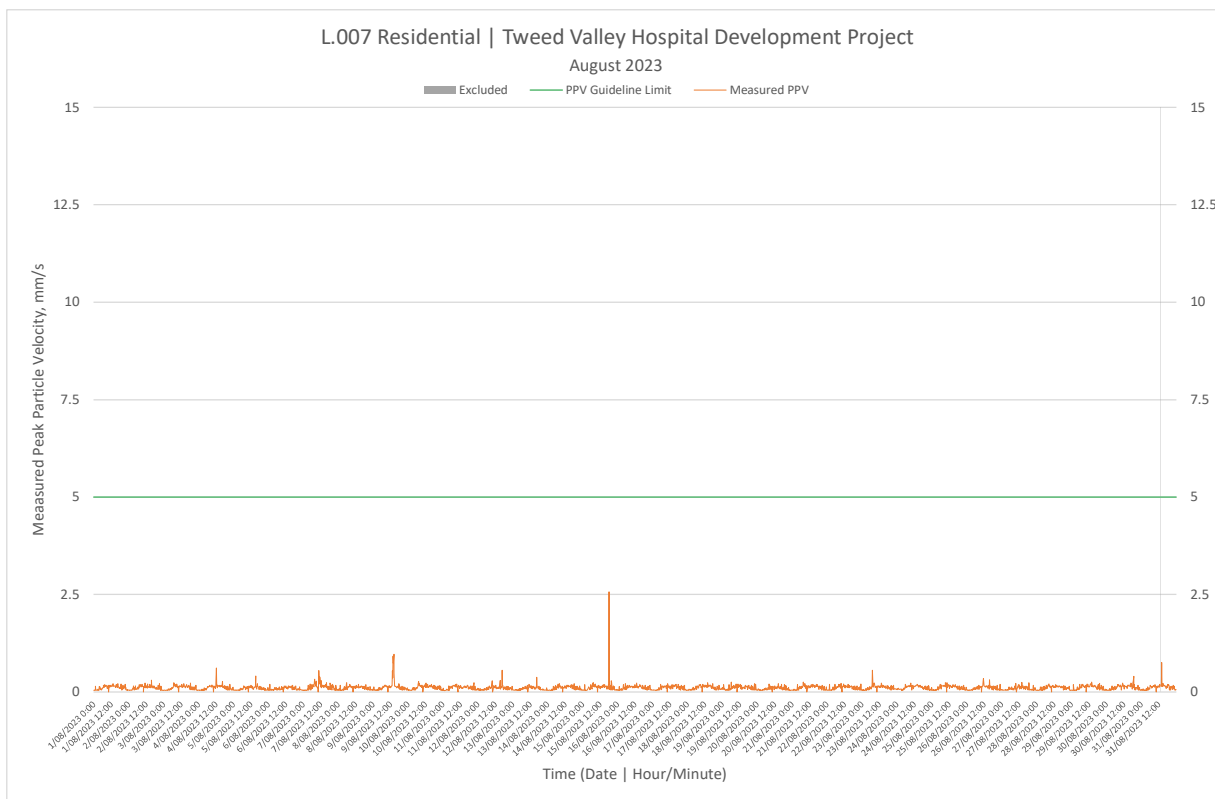


Figure 6 Velocity over time (Logger 007 – Residential)

Figure 7 illustrates the Frequency over Velocity for the data collected and analysed at Location L.007.

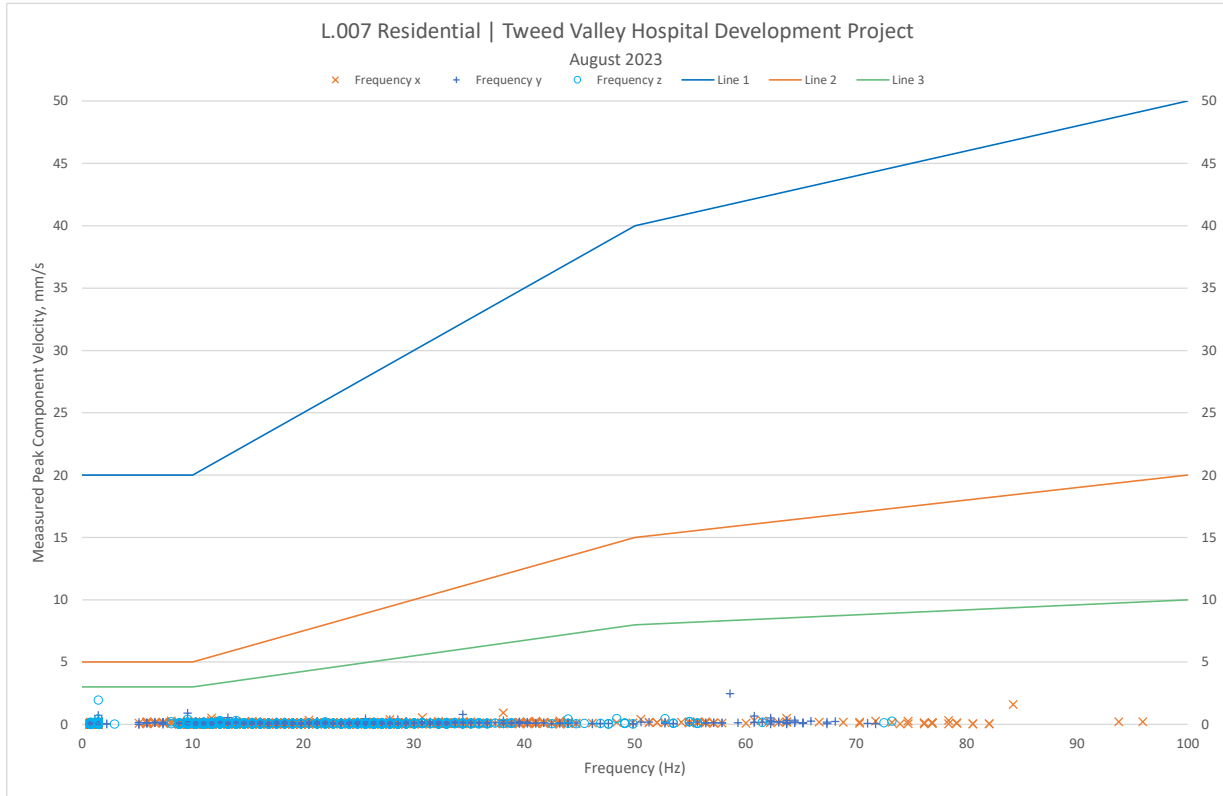


Figure 7 Frequency over Velocity (Logger 007 – Residential)

Throughout the survey period, each of the vibration loggers used during the monitoring survey have not recorded any velocity energy of any concern.

3.2.2 Acceleration/VDV

During August 2023, road works along Cudgen Road were undertaken where fewer heavy plant equipment operated along the alignment.

At each location, no reported acceleration or VDV levels of concern has been identified. The maximum VDV level measured across all locations is 0.1 m/s^{1.75} and no impact is noted.

Figure 8 below presents iVDV, accumulated VDV (per period), and weighted RMS Acceleration (α_{rms}) data measured at L.005.

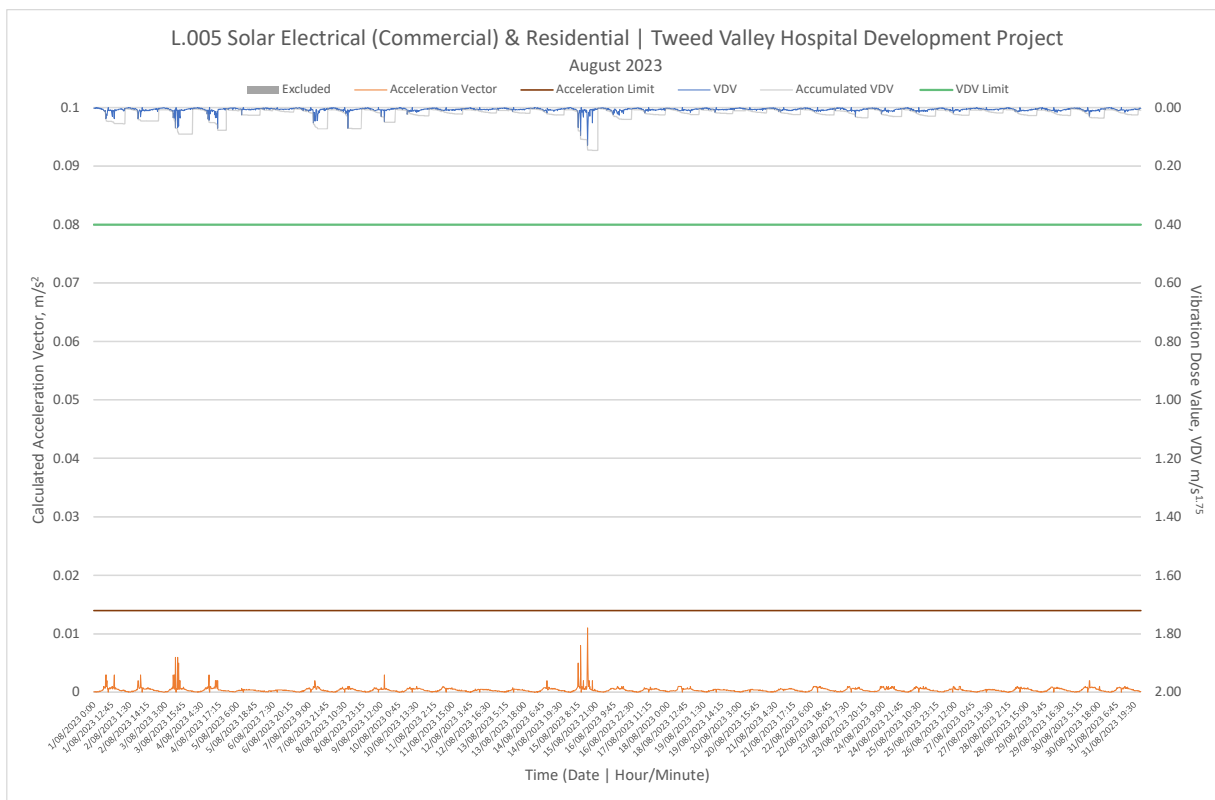


Figure 8 Acceleration and Vibration Dose Value over time (Logger 005)

The vibration impact at the commercial and residential premises is presented below in **Figure 9**.

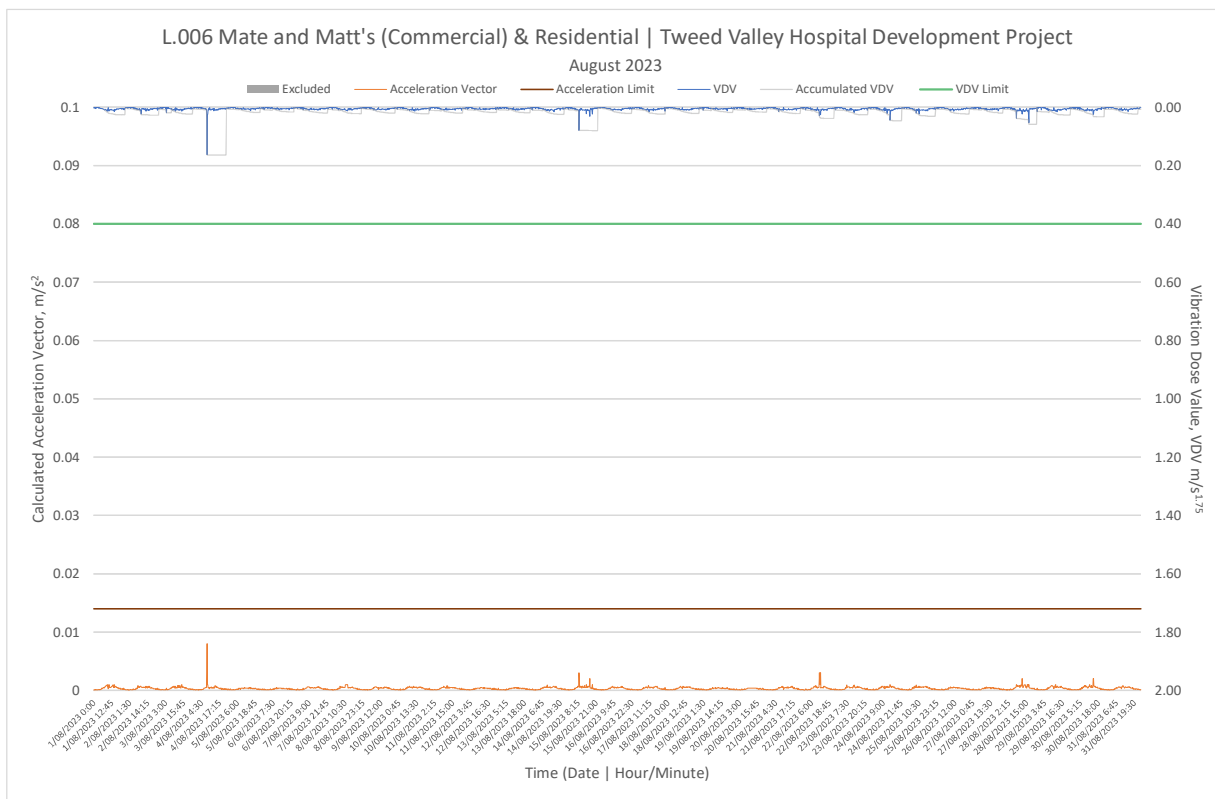


Figure 9 Acceleration and Vibration Dose Value over time (Logger 006 – Residential/Commercial)

Figure 10 which follows presents vibration dose at the southwestern residential receiver at Location L.007.

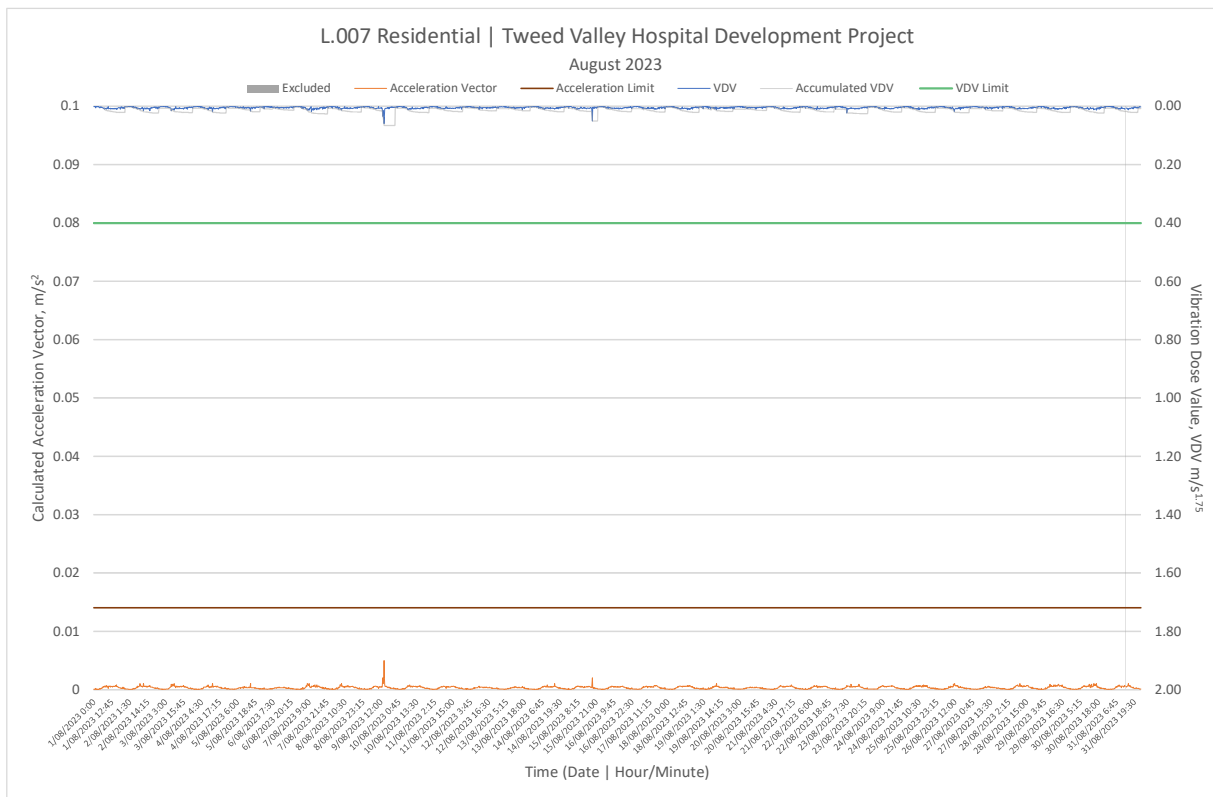


Figure 10 Acceleration and Vibration Dose Value over time (Logger 007 – Residential)

3.3 Discussion

Works proceeding during July include landscaping and traffic light installations. The measured vibration levels presented in this report are consistent with low vibration energy activities, none of which present any concern regarding velocity impact to structures, or dosage impact to human comfort.

Nil impact is recorded for July 2023.

4 Conclusion

ADE Consulting Group Pty Ltd (ADE) was commissioned by Lendlease Group (Lendlease) to assess the levels of construction related vibration during the construction of the Tweed Valley Hospital Project and associated roadworks, located at 771 Cudgen Road, Cudgen NSW (hereinafter referred to as 'the Site').

This report summarises vibration data collected at three locations, positioned along the South and southwest of Cudgen Road. At the time of preparing this report and the monitoring period which it covers (July 2023), CD Civil are on site completing planned road work activities on Cudgen Road. These works include landscaping and traffic light installation.

The results outlined in this report are summarised as follows:

- Velocity
 - No impact of concern
- Acceleration and Vibration Dose Values
 - No impact of concern.

Appendix I – Glossary

1 Sound Pressure Level

Defined as:

$$L_p = 10 \log_{10} \left(\frac{p^2}{p_{ref}^2} \right) \text{ dB}$$

In the above equation, p is the sound pressure fluctuation relative to atmospheric pressure, and p_{ref} is 20 microPascals (2×10^{-5} Pa), the approximate threshold of hearing.

Sound or noise is the sensation produced at the ear by small fluctuations in atmospheric pressure. Human ears are sensitive to changes to sound pressure over a wide range, from 20 microPascals to 60 Pascals, in lieu of using a linear scale to represent this range, a logarithmic scale is adopted to better handle

2 Sound Power Level

Sound power level cannot be directly measured using a microphone, it does not change with distance and is not influenced by atmospheric conditions. The sound power level refers to the total energy of the sound, and is reference to 1 Pico Watt.

3 Weighting and Loudness

The overall level of a sound is usually expressed as dB(A) and not dB. Weighting refers to the human ear's frequency response to sound. Typically, sound is measured with an A-weighted filter which reduces the significance of lower frequencies and very high frequencies, increasing the importance of mid-frequencies (500 Hz to 4 kHz), and being a good measure of the "loudness" of a sound.

A change of 1 to 2 dB(A) is difficult to detect, whilst a change of 3 to 5 dB(A) corresponds to a small but noticeable change. A 10 dB(A) change corresponds to a doubling or halving in apparent loudness.

4 Noise Metrics and Statistical Noise Levels

- i) L_{Aeq} - The time averaged A-weighted sound pressure level for the interval, as defined in AS1055.1. It is generally described as the equivalent continuous A-weighted sound pressure level that has the same mean square pressure level as a sound that varies over time. It can be considered as the average sound pressure level over the measurement period.
- ii) L_{Amin}/L_{Amax} - Minimum or Maximum A-weighted noise level detected during the measuring period. It refers to the minimum background noise detected or the maximum L_p measured.
- iii) L_{A90} - A-weighted noise level which is exceeded for 90% of the measuring period. It is usually

used as the descriptor for background noise level during the measurement period.

- iv) L_{A1} - Noise level which is exceeded for 1% of the measurement period.
- v) L_{A10} - Noise level which is exceeded for 10% of the measurement period. The L_{A10} is often referred to as the average *maximum* noise level.

5 Background Noise

The underlying level of noise present in the ambient noise, excluding the noise source which is under investigation, when extraneous noise is removed.

6 Ambient Noise

Ambient noise of an environment: the all-encompassing sound associated with that environment, being a composite of sounds from many sources.

7 Vibration

The mechanical oscillations occurring about an equilibrium point. The oscillations may be periodic such as the motion of a pendulum or random. Vibration is most commonly expressed in terms of displacement, velocity, acceleration and frequency, all of which are related

8 Displacement

The change in position of an object, is a vector quantity. (Stress indicator).

9 Velocity

The rate of change of displacement, is a vector quantity. (Fatigue indicator).

10 Acceleration

The rate of change of velocity, is a vector quantity. (Indicator of force).

11 Frequency

The number of times a periodic function or vibration occurs or repeats itself in a specified time, often 1 second – cycles per second. Frequency is measured in Hertz.

12 Hertz

The unit of frequency or pitch of a sound. One hertz equals one cycle per second.

13 Peak Particle Velocity (PPV)

The greatest instantaneous particle velocity during a given time interval if measurements are made in 3-axis. The resultant Peak Particle Velocity (PPV) is the vector sum i.e. the square root of the summed squares of the maximum velocities, regardless of when in the time history those occur.

14 Root Mean Square rms

The rms value of a set of numbers is the square root of the average of their squares. Best used when assessing building damage.

15 Vibration Dose Value VDV

The Vibration Dose Value (VDV) is used for assessing intermittent vibration. A cumulative measurement of the vibration level received over an 8-hour or 16-hour period. Best used when the structure is occupied.

16 Peak

The peak is the maximum amplitude during a measurement period.

17 Peak to Peak P-P

The peak-to-peak (P-P) is the difference between the maximum positive and maximum negative amplitudes of a waveform.

18 Logarithmic Scale

Comparing frequency with large amplitude differences be accomplished using a logarithmic scale. Critical vibration components usually occur at low amplitudes compared to the rotational frequency vibration. These components are not revealed on a linear amplitude scale because low amplitudes are compressed at the bottom of the scale, however a logarithmic scale shows prominent vibration components equally well at any amplitude.

19 Primary Waves P Waves

Alternating compressions ('pushes') and dilations ('pulls') in the same direction as the wave is propagating. P waves are the first arriving energy, smaller and higher frequency than S waves.

20 Secondary Waves S Waves

Alternating transverse motions perpendicular to the direction of propagation. Slower than P waves.

21 Rayleigh Waves R Waves

Motion is both in the direction of propagation and perpendicular (in a vertical plane). R waves are also dispersive, and amplitudes decrease with depth.

22 Accelerometer

A vibration sensor whose electrical output is directly proportional to the acceleration component of the vibration. The two most common accelerometer types are the traditional charge type and the IEPE, integrated electronic piezoelectric type with a built-in line-drive amplifier to enable the output signal to be transmitted over 'longer cable runs'.

23 Geophone

Geophones measure velocity by means of a magnetic core surrounded by an electrical coil. When the surface vibrates, the geophone housing moves however the coil stays stationary, thus the movement of the magnet in the coil causes an electrical current which is calibrated to velocity of vibration.

24 Short-term vibration

Vibration which does not occur often enough to cause structural fatigue, and which does not produce resonance in the structure being evaluated.

25 Long-term vibration

All types of vibration not covered by the definition of 'short-term vibration'

26 Impulsive vibration

Rapid build-up to a peak followed by a damped decay that may or may not involve several cycles of vibration. It can also consist of a sudden application of several cycles at approximately the same amplitude, providing that the duration is short (typically <2 seconds). Impulsive vibration (no more than 3 occurrences) in an assessment period is assessed on the basis of weighted rms acceleration, and peak particle velocity.

27 Continuous vibration

Continuous vibration continues uninterrupted for a defined period (usually throughout daytime and/or night-time). This type of vibration is assessed on the basis of weighted rms acceleration.

28 Intermittent vibration

Defined as interrupted periods of continuous (e.g., a drill) or repeated periods of impulsive vibration (e.g., a pile driver), or continuous vibration that varies significantly in magnitude. It may originate from impulse sources (e.g., pile drivers and forging presses) or repetitive sources (e.g. pavement breakers), or sources which operate intermittently, but which would produce Continuous vibration if operated continuously (for example, intermittent machinery, railway trains and traffic passing by). This type of vibration is assessed on the basis of vibration dose value.

Appendix II – Aerial Photograph

ADE Monitoring locations, site location (including CD Civil's Cudgen Road Upgrade works) are presented below.



Appendix III – References

Standards, policies, and guidelines used for the assessment of vibration are as follows:

- ADE Group Consulting Pty Ltd – Cudgen Road Upgrade Construction Noise and Vibration Impact Statement, Prepared for CD Civil, Version 1.0, 6 September 2022 (ADE Reference A103022.1044.00)
 - Addendum v1.1f, April 2023
- Assessing Vibration: A Technical Guideline (February 2006), Department of Environment and Conservation (DEC)
- British Standard BS 7385-2:1993 Evaluation and measurement for vibration in buildings – Part 2: guide to damage Levels from ground-borne vibration
- British Standard BS 6472:2008 Guide to evaluation of human exposure to vibration in buildings – Part 1: vibration sources other than blasting
- Construction Noise and Vibration Strategy (April 2019) Published by Transport for New South Wales (TfNSW)
- Development Consent SSD-10353, Department of Planning, Industry and Environment – Tweed Valley Hospital Stage 2 – 12 July 2020 (approval)
- German Standard DIN 4150-1:2001 Structural vibration Part 1: Prediction vibration parameters
- German Standard DIN 4150-3:2016 Vibrations in buildings – Part 3: Effects on structures
- Tweed Valley Hospital Management Plan – Noise and Vibration, Revision 7.0, Lendlease Building Pty Ltd, 11 June 2019
- Tweed Valley Hospital – Noise and Vibration Impact Assessment for State Significant Development (SSD), SVM-2370, Revision: Issue 2, 17 October 2018 – Acoustic Studio

Appendix IV – Site Photographs



Photograph 1 Representative photograph of monitoring location 007 – Residential, as observed 17/04/2023



Photograph 2 Representative photograph of monitoring location 005 – Solar Industry, as observed 17/04/2023



Photograph 3 Representative photograph of monitoring location 006 – Mate and Matts, as observed 17/04/2023

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Tweed Valley Hospital 771 Cudgen Road, Cudgen NSW

Document ID | A101021.0286.00 VIB49 v0.1d



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