

Vibration Monitoring Assessment Report

771 Cudgen Road, Cudgen NSW

Prepared for: Lendlease Building Pty Ltd

Job Number: A101021.0286.00 VIB44.Rev0 | Date: 11/04/2023



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For and on behalf of

ADE Consulting Group Pty Ltd

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Executive Summary

ADE Consulting Group Pty Ltd (ADE) was commissioned by Lendlease Group (Lendlease) to assess the levels of construction related vibration during the construction of the Tweed Valley Hospital Project, located at 771 Cudgen Road, Cudgen NSW.

This report summarises vibration data collected at three (3) locations during the monitoring period of March 2023 with the monitoring devices positioned to the south and southwest of Cudgen Road. At the time of preparing this report and the monitoring period in which it covers (March 2023), CD Civil are on site undertaking planned road work activities on Cudgen Road, and Lendlease are completing superstructure works.

The road works and associated auxiliary construction activities underway are in close proximity to the vibration loggers, each of which is positioned in close proximity to residential receivers. These receivers are anticipated to experience some increased levels of perceptible vibration at which the occupants' comfort may be impacted during vibration intensive works.

Higher levels of vibration were measured during this monitoring period. Works occurring close to sensitive receivers along Cudgen Road may experience an increase in vibration energy during these close proximity works. Human comfort may be impacted where high intensity vibration producing equipment is expected to be utilized to complete the road works, and prolonged use of heavy plant equipment on grounds considered to be comprised predominately of softer soils.

While the impact at the loggers would be higher than at the facade or foundation of the receiver, the data presented in this report shows the potential for impact which may induce a community response to the works.

ADE prepared a Construction Noise and Vibration Impact Statement to CD Civil which presents mitigation measures and management practices for impacted receivers (where feasible and reasonable). To date, no comment or complaint has been received from the receivers.

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1 Introduction

1.1 Introduction

ADE Consulting Group Pty Ltd (ADE) was engaged by the Lendlease Group (Lendlease) to assess the levels of construction related vibration during the construction of the Tweed Valley Hospital Project and associated road upgrades located at 771 Cudgen Road, Cudgen in New South Wales (hereinafter referred to as ‘the Site’).

No one section or part of a section of this report should be taken as giving an overall idea of this report. Each section must be read in conjunction with the entire report, including its appendices and attachments.

At the time of vibration monitoring, Lendlease was continuing superstructure works on the Site which included the construction of columns and suspended slabs. Concurrently CD Civil were undertaking roadworks associated with the development on Cudgen Road which included the construction of an intersection for the new hospital development, construction of permanent footpaths, stormwater drainage construction (trenching works), road pavement and widening.

The road improvement works include the use of large 10T vibratory rollers, multi-tyred rollers, generators, excavators, graders and asphalt machines.

The purpose of environmental monitoring is to:

- Assess construction related ground borne vibration levels against regulatory requirements, development consent conditions, Australian guidelines, and international standards for construction vibration management and control on construction sites.
- Manage and mitigate potentially excessive vibration generation through site planning and the adoption of appropriate work methods and practices where feasible and reasonable.
- Monitor and assess construction impacts likely to cause adverse comment by the community or impact surrounding sensitive receivers/structures, and provide feasible and reasonable recommendations to manage the impacts.
- Establish and maintain positive relationships with project stakeholders.

The purpose of the Vibration Monitoring Assessment (NVA) report is to assess the potential impacts arising from construction activities associated with the Tweed Valley Hospital Project, with a particular focus on vibration levels on site to ensure they comply with the Tweed Valley Hospital– Noise and Vibration Management Plan.

The main objective is to minimize the vibration impacts that have been identified and preserve the public amenity of the local area during construction. This aligns with the conditions C18 – C20 and B16 outlined in the development consent, which are summarized in Section 1.2.1, as well as the relevant goals specified in Section 2. The primary focus is to adhere to the Development Consent and Guidelines in order to achieve these objectives.

A general vibration and acoustic glossary is provided in **Appendix I – Glossary**.

1.2 Project background

On 13 June 2017, the NSW Government announced an allocation of approximately \$534M for the development of a new hospital on a greenfield site in the Tweed Valley area. The site of the new Tweed Valley Hospital (the Project) is located at 771 Cudgen Road, Cudgen in New South Wales.

An Environmental Impact Statement (EIS) was prepared to accompany a State Significant Development Application for the Project which was assessed under Part 4 of the *Environmental Planning and Assessment Act 1979* (EP&A Act).

An overview of the project specific information is provided in **Table 1** below.

Table 1 Project Specific Information

| Site Details | |
|----------------------------|--|
| Client Name: | Lendlease |
| ADE Project Number: | A101021.0286.00 |
| Site Address: | 771 Cudgen Road, Cudgen NSW (Lot 11 DP 1246853) |
| Date of Report: | 01/06/2023 |
| Development Consent | SSD-10353, Health Administration Corporation. Authorized by the Minister for Planning and Public Spaces on 9 March 2020. Consent approved on 12 June 2020. |
| Objectives: | <ul style="list-style-type: none"> Comply with DIN 4150-3:2016 guidelines and conditions C18 - C20 of Development Consent SSD-10353 Manage potential vibration impacts from construction activities which have the potential to affect the nearby buildings (Kingscliff TAFE and residential properties) To manage the generation of vibration which could affect the neighbours of the Site, workers on the Site, associated buildings, and other members of the public Establish and maintain good relationships with the neighbours and wider community. |
| Key Legislation: | <p>Protection of the Environment Operations Act 1997 (NSW) (POEO Act).</p> <p>The POEO Act is a key piece of environmental protection legislation and regulates activities via:</p> <ul style="list-style-type: none"> Environmental protection licensing, as per schedule 1 Regulation of scheduled and non-scheduled activities Environmental protection offences and penalties Establishment of a <i>general duty of care</i> to notify <i>environment harm</i>. |

1.2.1 Development consent SSD-10353

The consent of approval conditions regarding vibration are summarised below in **Table 2**.

Table 2 Development Consent Conditions

| Condition of Approval number | Detail of Condition Requirement |
|------------------------------|---|
| C18 | <p>Vibration caused by construction at any residences or structure outside the site must be limited to:</p> <ol style="list-style-type: none"> For structural damage, the latest version of DIN 4150-3 (1992-02) Structural Vibration- Effects of vibration on structures (German Institute for Standardisation, 1999) For human exposure, the acceptable vibration values set out in the Environmental Noise Management Assessing Vibration: A Technical Guideline (DEC, 2006) (as may be updated or replaced from time to time) |
| C19 | Vibratory compactors must not be used closer than 30 m from residential buildings unless vibration monitoring confirms compliance with the vibration criteria specified in <i>Condition C18</i> |
| C20 | The limits in conditions C18 and C19 apply unless otherwise outlined in the CNVMSP, approved as part of the CEMP required by <i>Condition of Approval (CoA) B16</i> of this consent |

Note: CoA B16 refers to an approved condition stated in the Lendlease's Construction Noise and Vibration Management Sub-Plan (CNVMSP)

1.2.2 Monitoring Locations

The vibration monitoring equipment was relocated on 17 November 2022 along the southern alignment of Cudgen Road at three designated locations (ie Monitoring Location 005, 006 & 007) prior to the commencement of roadworks.

The monitoring locations were established to assess the potential vibration impacts to the nearest sensitive receivers and comply with the requirements and conditions set out in the Tweed Valley Hospital– Noise and Vibration Management Plan.

All monitoring locations are within close proximity to the boundary of the nearest sensitive receivers (residential and commercial) that may be impacted by vibration generated from the current roadworks program and associated plant.

The aerial imaging and monitoring location overview is presented in **Appendix II – Aerial Photograph**.

2 Vibration guidelines summary

Vibration criteria and guidelines values for sensitive structures and human comfort are derived from Australian guidelines and International Standards for the purpose of assessment.

2.1 Guideline vibration values

International standards from Germany and the United Kingdom are used in conjunction with the NSW guideline *Assessing Vibration: A Technical Guideline* (DEC, 2006) for assessment of measurement data. The DEC guideline is an informal guideline for assessment of vibration under Australian conditions. The document outlines, summarizes, and provides guidance for the assessment of vibration.

The International Standards and the DEC guideline provide best practice assessment for intermittent or transient and continuous vibration that is commonly generated by construction and roadwork activity.

These standards and guidelines offer guidance for the assessment of:

- Human perception to vibration
- Structures sensitive to vibration
 - Residential buildings
 - Commercial
 - Heritage or other sensitive buildings
 - Buried pipework or other utility services including concrete and masonry.

2.1.1 Structural/Cosmetic damage

For the assessment of the potential for vibration induced damage (structural or cosmetic) of buildings, the German Standard DIN4150-3:2016 is primarily used when examining the vulnerability of ground-related services and structures to vibration.

The DIN criteria have been adopted for building damage as they are more stringent and although they vary based on the frequency range of the predominant pulse can be summarised as 5 mm/s for residential dwellings.

Table 3 below provides guideline values for evaluation of long-term vibration on buildings.

Table 3 Guideline values for evaluating the long-term vibration effects on buildings

| Type of building | Guideline values for $v_{i, \max}$ mm/s (PPV) | |
|---|--|---|
| | Topmost floor, horizontal direction, all frequencies | Floor slab, vertical direction, all frequencies |
| Buildings used for commercial purposes, industrial buildings, and buildings of similar design | 10 | 10 |
| Residential buildings and buildings of similar design and/or occupancy | 5 | 10 |
| Structures that, because of their particular sensitivity to vibration, cannot be classified as above and are of great intrinsic value (e.g. listed buildings) | 3 | 10 |

Note: Bold represents project-specific vibration guidelines

Short term vibration includes works such as impact pile driving, excavation, and rock breaking which would cause impulsive or intermittent vibration impacts on the surrounding receivers and is assessed as transient PPV vibration. Guidance is taken from the DIN 4150 standard.

Table 4 below provides guidance for values for Peak Particle Velocity (PPV) at the foundation of the structure and at the plane of the topmost floor. Table 4 illustrates particle velocity and damage (cosmetic or structural) and is frequency dependent (ie that the lower the frequency the more sensitive the structure may be to vibration).

Table 4 Guideline Values for Vibration Velocity (Evaluating Effects of Short-Term Vibration on Structures)

| Line | Type of Structure | Peak Particle Velocity, mm/s | | | | |
|------|---|---------------------------------|-------------|--------------|-------------------------------------|---------------------------------|
| | | At foundation at a frequency of | | | Highest floor, horizontal direction | Floor Slabs, vertical direction |
| | | 1 to 10 Hz | 10 to 50 Hz | 50 to 100 Hz | All Frequencies | All Frequencies |
| 1 | Buildings used for commercial purposes, industrial buildings and buildings of similar design | 20 | 20 to 40 | 40 to 50 | 40 | 20 |
| 2 | Dwellings and buildings of similar design and/or occupancy | 5 | 5 to 15 | 15 to 20 | 15 | 20 |
| 3 | Structures that, because of their particular sensitivity to vibration, cannot be classified under lines 1 and 2 and are of great intrinsic value (e.g. listed buildings under preservation order) | 3 | 3 to 8 | 8 to 10 | 8 | 20 |

Note: Bold represents project-specific vibration guidelines

A graphical representation of **Table 4** is shown below in **Figure 1**.

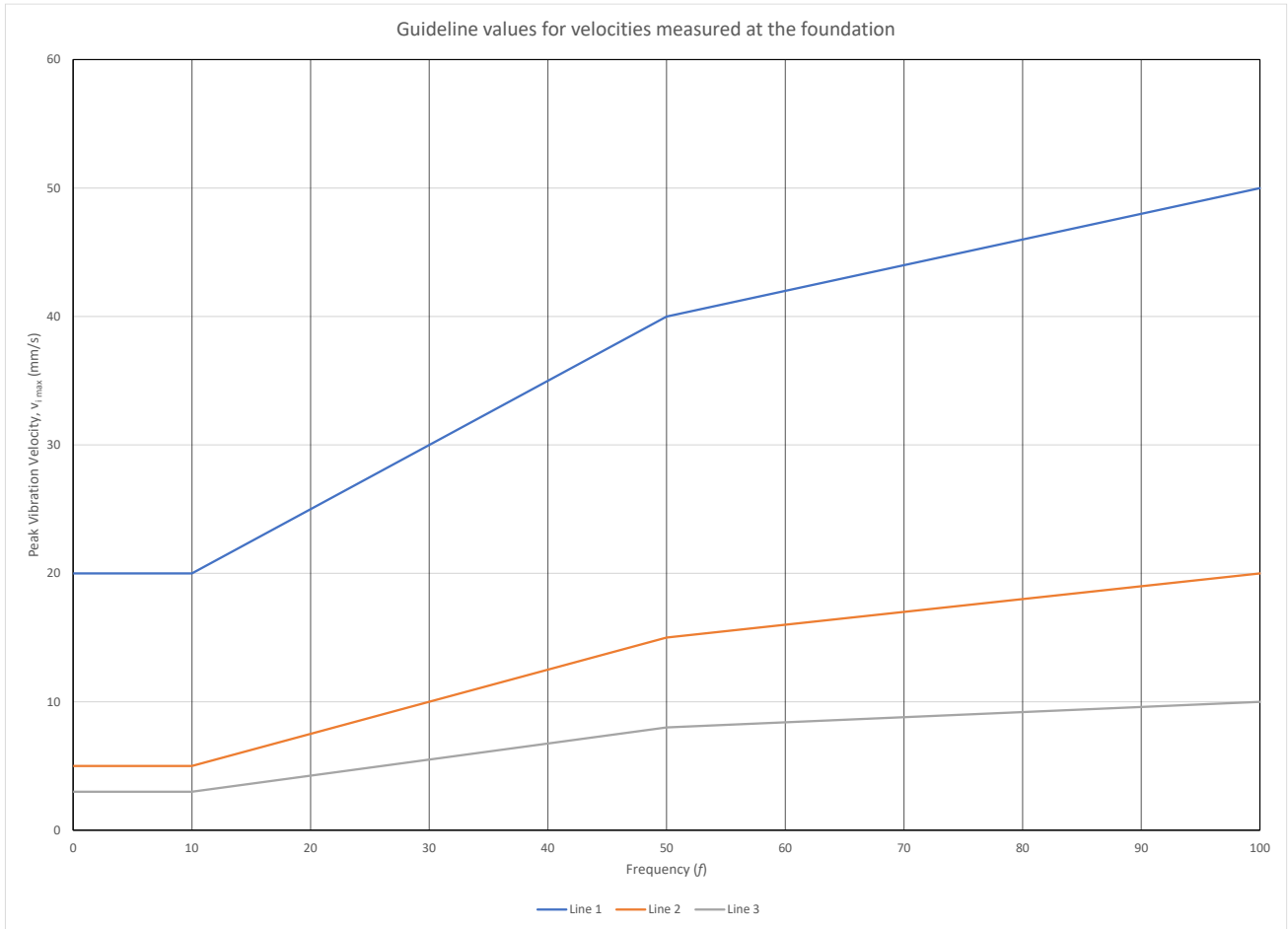


Figure 1 Illustration of the DIN4150 guideline. Structural sensitive to vibration is a function of frequency and velocity

2.1.2 Safe working distances

The Construction Noise and Vibration Strategy (CNVS, TfNSW 2019) outlines the minimum safe working distances for vibration intensive plant for surrounding vibration sensitive receivers.

As a guide, the minimum working distances for typical vibration intensive plant are listed in **Table 5**. These minimum working distances are summarised for both cosmetic damage (BS 7385 and DIN 4150) and human comfort (*Assessing Vibration: A Technical Guideline*).

Table 5 Recommended minimum working distances from vibration intensive plant (TfNSW CNS)

| Plant Item | Approximate Size / Weight / Model | Minimum Distance for Cosmetic Damage (BS7385) | Minimum Distance for Human Response (DEC Assessing Vibration) | Heritage (DIN4150) |
|-------------------------|-----------------------------------|---|---|--------------------|
| Vibratory Roller | 1-2 tonne | 5 m | 15 – 20 m | 11 m |
| | 2-4 tonne | 6 m | 20 m | 14 m |
| | 4-6 tonne | 12 m | 40 m | 27 m |
| | 7-13 tonne | 15 m | 100 m | 33 m |
| | 13-18 tonne | 20 m | 100 m | 44 m |
| | >18 tonne | 25 m | 100 m | 55 m |
| Small Hydraulic Hammer | 300 kg (5 to 12t excavator) | 2 m | 7 m | 5 m |
| Medium Hydraulic Hammer | 900 kg (12 to 18t excavator) | 7 m | 23 m | 16 m |
| Large Hydraulic Hammer | 1600 kg (18 to 34t excavator) | 22 m | 73 m | 49 m |
| Pile Driver – Vibratory | Sheet piles | 2 to 20 m | 20 m | 15 m ^B |
| Piling Rig - Bored | ≤ 800 mm | 2 m (nominal) | n/a | 6 m ^A |
| Piling Rig – Hammer | 12 t down force | 15 m | 50 m | 45 m ^A |
| Jackhammer | Hand held | 1 m | Avoid contact with structure | 3 m |

Note: Where works occur closest to a sensitive receiver which is designated as a heritage structure, more stringent conditions may apply. For this, a conservative minimum cosmetic damage distance multiplied by 2.2 is used as a guide only

Note A: Data taken from BS5228-2:2009

Note B: Conservative estimate

2.1.3 Human comfort

Construction activities which have the potential to create ground-borne vibrations may impact sensitive receivers near the project works. Humans are responsive to vibration and some discomfort may arise due to various construction related activities and their intensity/duration.

For assessment of human comfort and exposure to vibration, the NSW document *Assessing Vibration: A Technical Guideline* (DEC, 2006) provides direction derived from the British Standard BS6472-1:2008 *Guide to evaluation of human exposure to vibration in buildings. Part 2: Vibration sources other than blasting*.

Table 6 below tabulates the Vibration Dose Values (VDV) for human comfort. These values represent a guideline for the total accumulation of vibration energy during a 15-hour day-time period where the vibration would be experienced. VDV is the total accumulated energy over time.

Table 6 Vibration Dose Values (VDV) for Intermittent Vibration

| Location | Period | Preferred value, VDV m/s ^{1.75} | Maximum value VDV m/s ^{1.75} |
|--|--------------|---|--|
| Critical areas | Day or Night | 0.1 | 0.2 |
| Residences | Day | 0.2 | 0.4 |
| | Night | 0.13 | 0.26 |
| Offices, schools, educational institutions and places of worship | Day or Night | 0.4 | 0.8 |
| Workshops | Day or Night | 0.8 | 1.6 |

Note: Daytime is 07:00 am to 22:00 pm
 A 16 hour dosage is used for daytime to assess the dosage of vibration for a whole-day
 Note: **Bold** indicates project-specific relevance

Table 7 below tabulates guideline VDV ranges in residential buildings at which a human response or adverse comment to construction vibration would be likely. These levels are derived from BS6472-2 and provide a subjective judgement for which vibration onsite may result in adverse comment by those who experience it, and to which this monitoring report is assessed against.

Table 7 Vibration Dose Value ranges which might result in various probabilities of adverse comment within residential buildings

| Place and time | Low probability of adverse comment ¹ m/s ^{1.75} | Adverse comment possible m/s ^{1.75} | Adverse comment probable ² m/s ^{1.75} |
|----------------------------------|--|---|--|
| Residential buildings 16 hr day | 0.2 to 0.4 | 0.4 to 0.8 | 0.8 to 1.6 |
| Residential buildings 8 hr night | 0.1 to 0.2 | 0.2 to 0.4 | 0.4 to 0.8 |

Note 1: Below these ranges adverse comment is not expected
 Note 2: Above these ranges adverse comment is likely
 Note 3: For offices and workshops, multiplying factors of 2 and 4 respectively should be applied to the above vibration dose ranges for 15h day.

At levels within the ranges tabulated above, the probability for which a comment may be made from the community increases with increased vibration energy from the site. The degree of the dosage would determine the nature of the vibration perceived which may be experienced by occupants of nearby vibration sensitive receivers.

3 Results overview

3.1 Survey instrumentation and methodology

To assess the potential impacts and ground-borne vibration generated from the current works program, vibration measurements were recorded at three (3) locations in the March 2023 monitoring period. The equipment deployed and utilized at these three monitoring locations were Class 1 four-channel Svantek SVAN 958A Sound & Vibration Analysers.

These vibration monitors were enclosed in a weather resistant environmental case which is placed on the ground and covered with a tarp to aid in keeping temperatures below 60°C to prevent temperature related failures, and moisture intrusion. Images relating to the installation of the loggers is provided in **Appendix II – Aerial Photograph** and **Appendix IV – Site Photographs**.

The tri-axial accelerometer is placed firmly against the soil surface and covered with a sandbag to minimize external interference. The monitors are positioned external to the Site, along the boundary adjacent Cudgen Road to the south and southeast.

A summary of the vibration monitoring equipment is provided in **Table 8** below.

Table 8 Vibration equipment deployed

| Make | Model | Location | Serial Number | Calibrated on | Calibration Due |
|---------|----------|----------|---------------|---------------|-----------------|
| Svantek | SVAN958A | 005 | 92832 | 1/02/2022 | 1/02/2024 |
| Svantek | SVAN958A | 006 | 92835 | 18/02/2022 | 18/02/2024 |
| Svantek | SVAN958A | 007 | 92834 | 9/03/2022 | 9/03/2024 |

Lendlease has established a daily check list on site to ensure all monitors are operating in the field correctly, have adequate sunlight to power the units and that they are reporting consistently. Lendlease will report any issues immediately to ADE.

Furthermore, ADE conducts regular checks throughout the week via telemetry to ensure the monitors are operating and recording correctly with ADE to advise Lendlease of any issues immediately. Monitors will not be removed unless consultation with Lendlease, TSA Management and Health Infrastructure have occurred and alternative locations are agreed upon.

3.2 Results

3.2.1 Velocity

An increase in vibration intensive activities occurring along Cudgen Road during the road’s upgrade works has increased the energy recorded and measured at the ground sensors location. Peak events infrequently exceed the recommended velocity levels *at the sensor* and may be likely to exceed at the receiver in some minor instances, however low to no impact is likely based on data analysis.

The increase in construction activities utilizing heavy plant equipment is the origin of the measured energy, however ADE acknowledges that Logger L.006 is positioned near a farm field with irrigation which may influence both noise and vibration readings. In addition, trenching and grading activities proceeded throughout March at this location in close proximity to the devices.

Figure 2 below presents the velocity (PPV mm/s) at Location L.005 situated by a residential and commercial receiver.

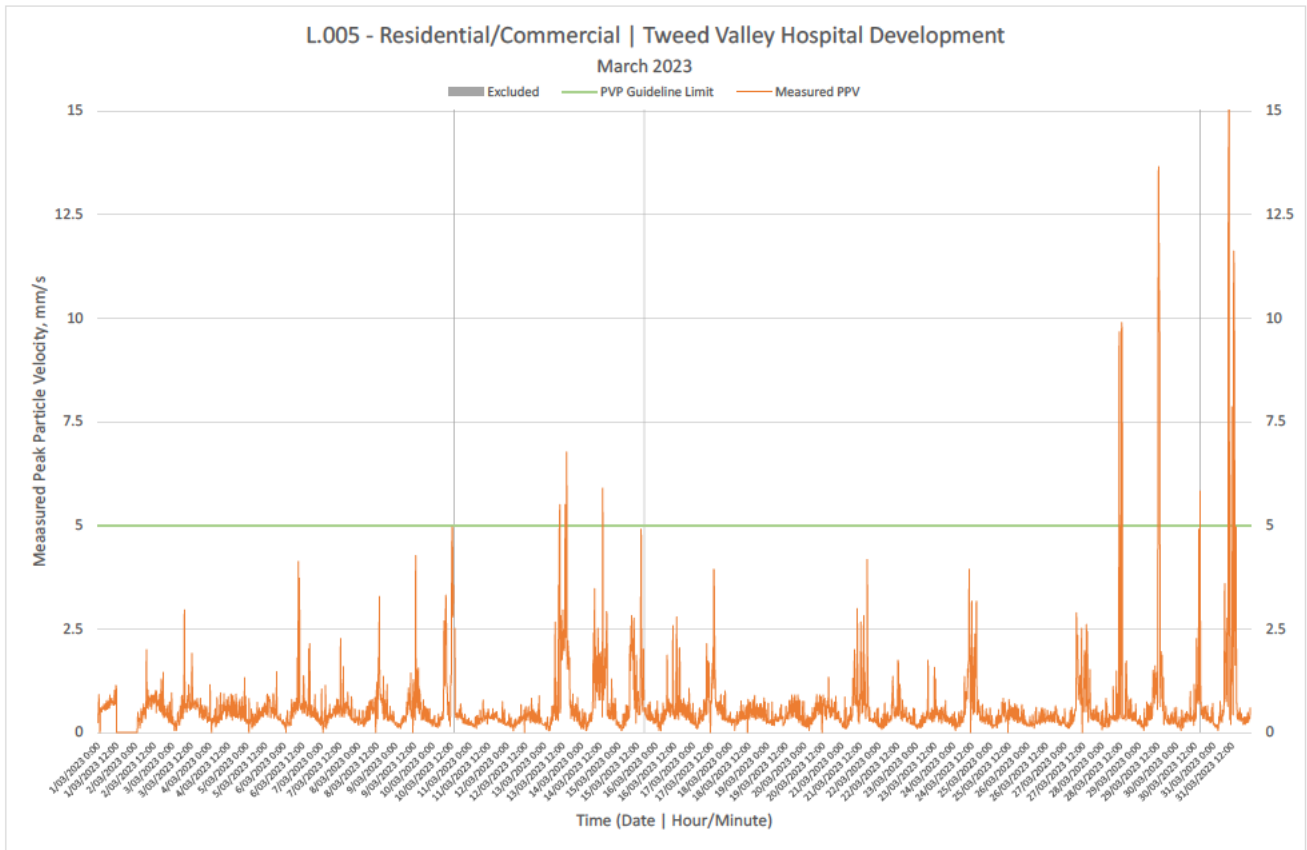


Figure 2 Velocity over time (Logger 005 - Residential/Commercial)

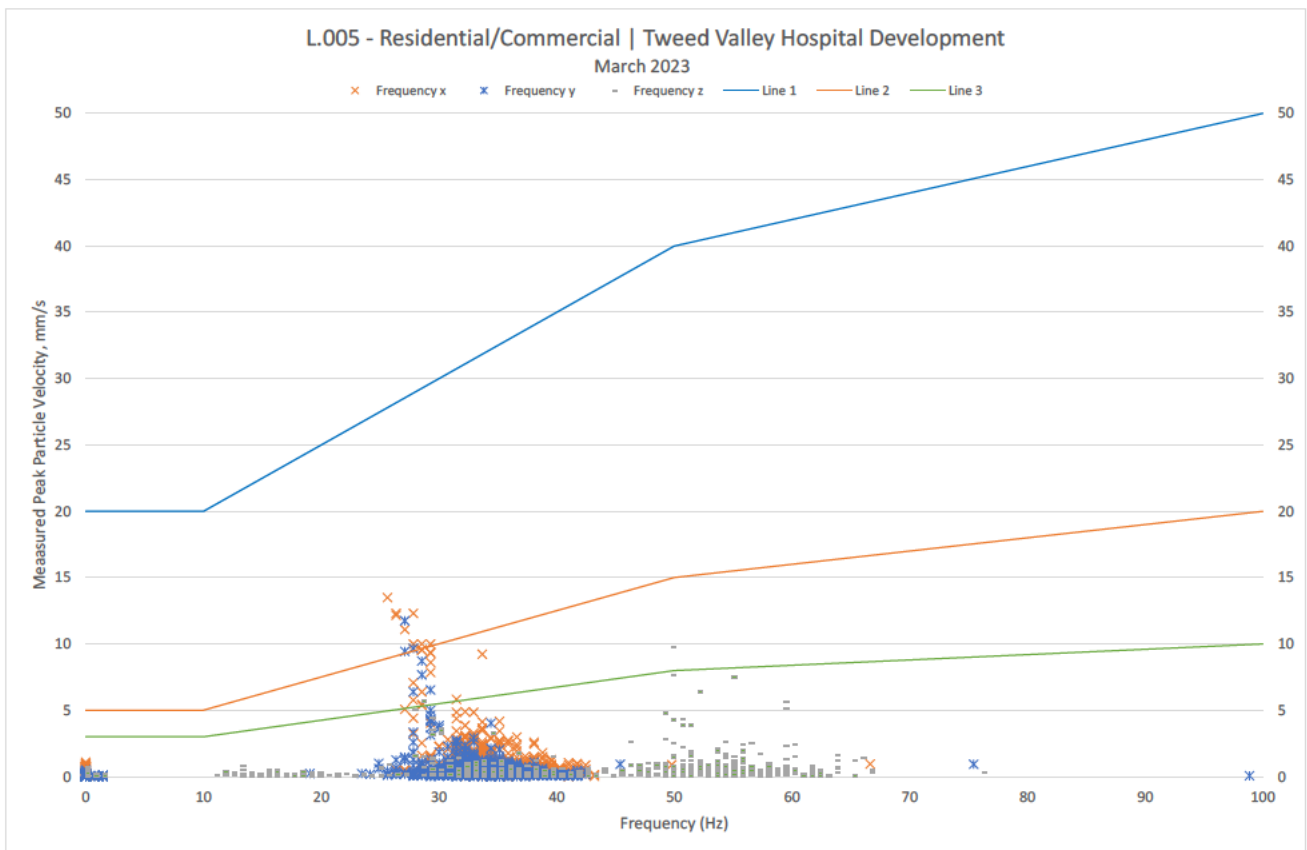


Figure 3 Frequency over Velocity (Logger 005 – Residential/Commercial)

Figure 4 below presents velocity measurement data measured at the Mate and Matts commercial/residential premises, nominated as Location L.006.

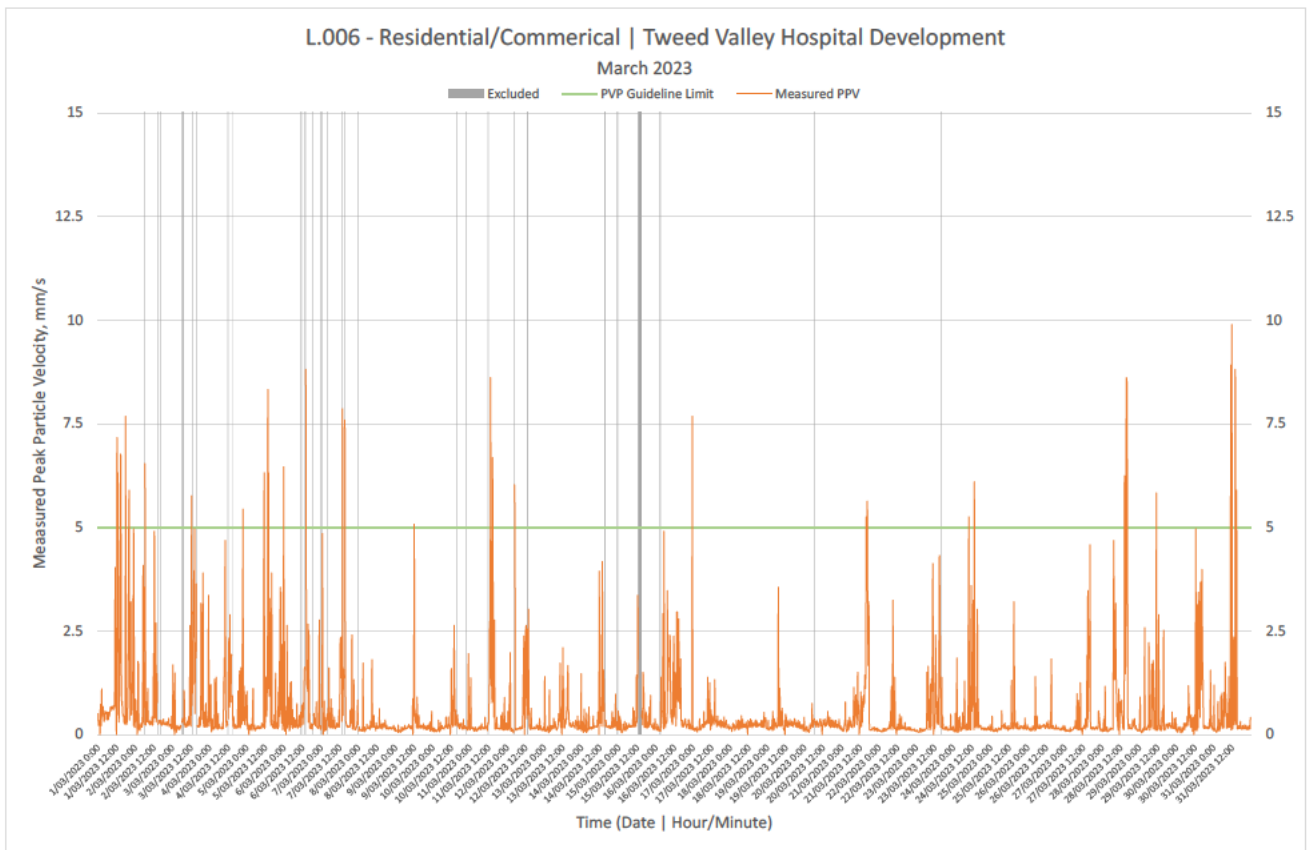


Figure 4 Velocity over time (Logger 006 – Residential/Commercial)

Works near the sensor and farm/commercial related events are judged to be the likely origin of the increase in vibration energy at this location. Grading works were in close proximity to the device throughout March, as noted in the photograph provided in Figure 5.



Figure 5 Image: L.006 in close proximity to works, 13 March 2023 15:52 hrs

Trenching works utilizing an 8T tracked excavator with a bucket attachment and 5T roller was in use in distances of approximately 2 - 10 m from the vibration sensor.

Other identified sources of vibration energy include equipment (some of which may not be related to the road works) being dropped, placed, or moved at very close proximity (<2 m) from the enclosure and the vibration ground sensor has been documented by ADE staff during routine site visits.

Figure 6 below illustrates the frequency for each axis over the velocity of each axis for Logger L.006. The data shows that high frequency over low velocity is indicative of extraneous data captured at the site, and likely not of site origin.

In regards to cosmetic damage or structural concerns, no impact to any of the structures near to this location is anticipated as frequency thresholds are lower than the limitations outlined in both the British and German Standards.

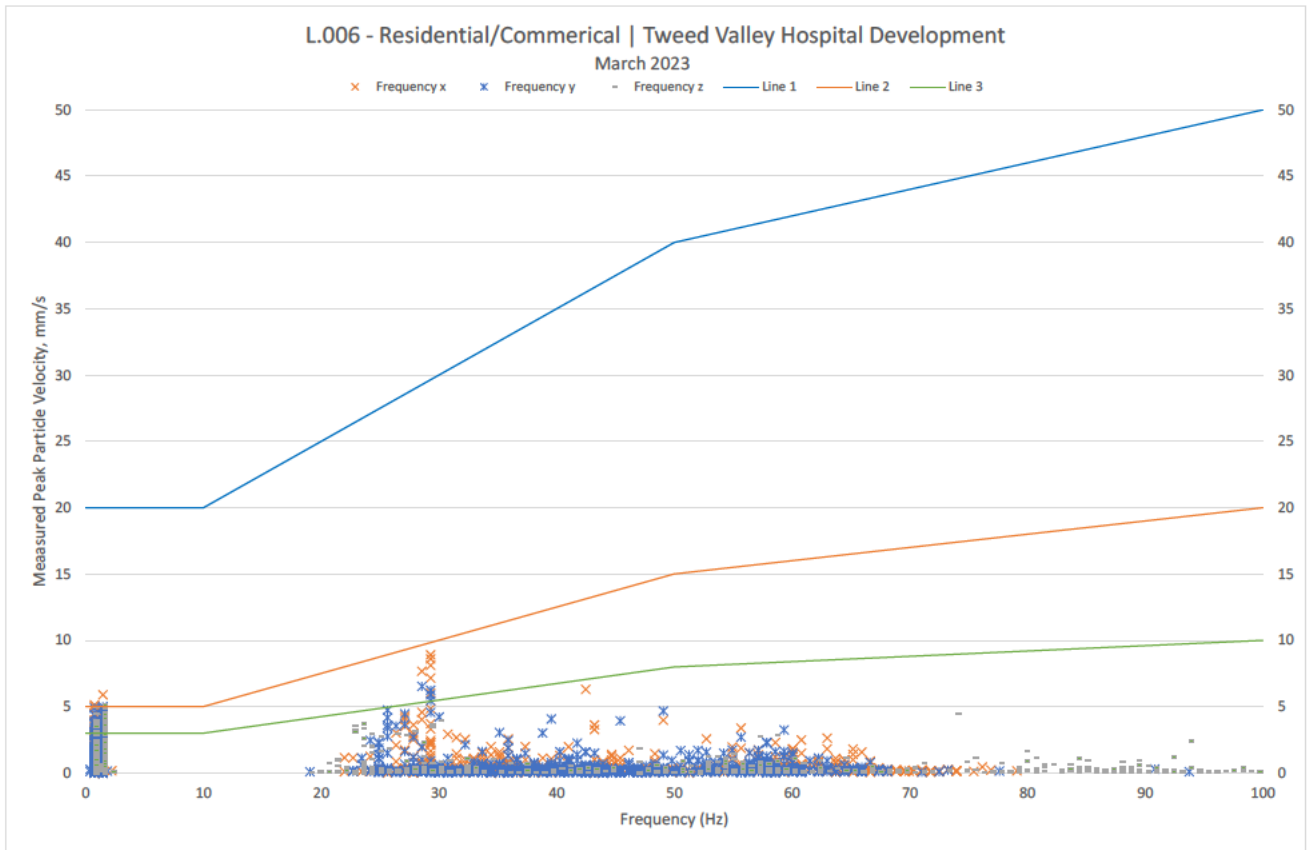


Figure 6 Frequency over Velocity (Logger 006 – Residential/Commercial)

Figure 7 below presented velocity data for the logger located in close proximity to a residential premises.

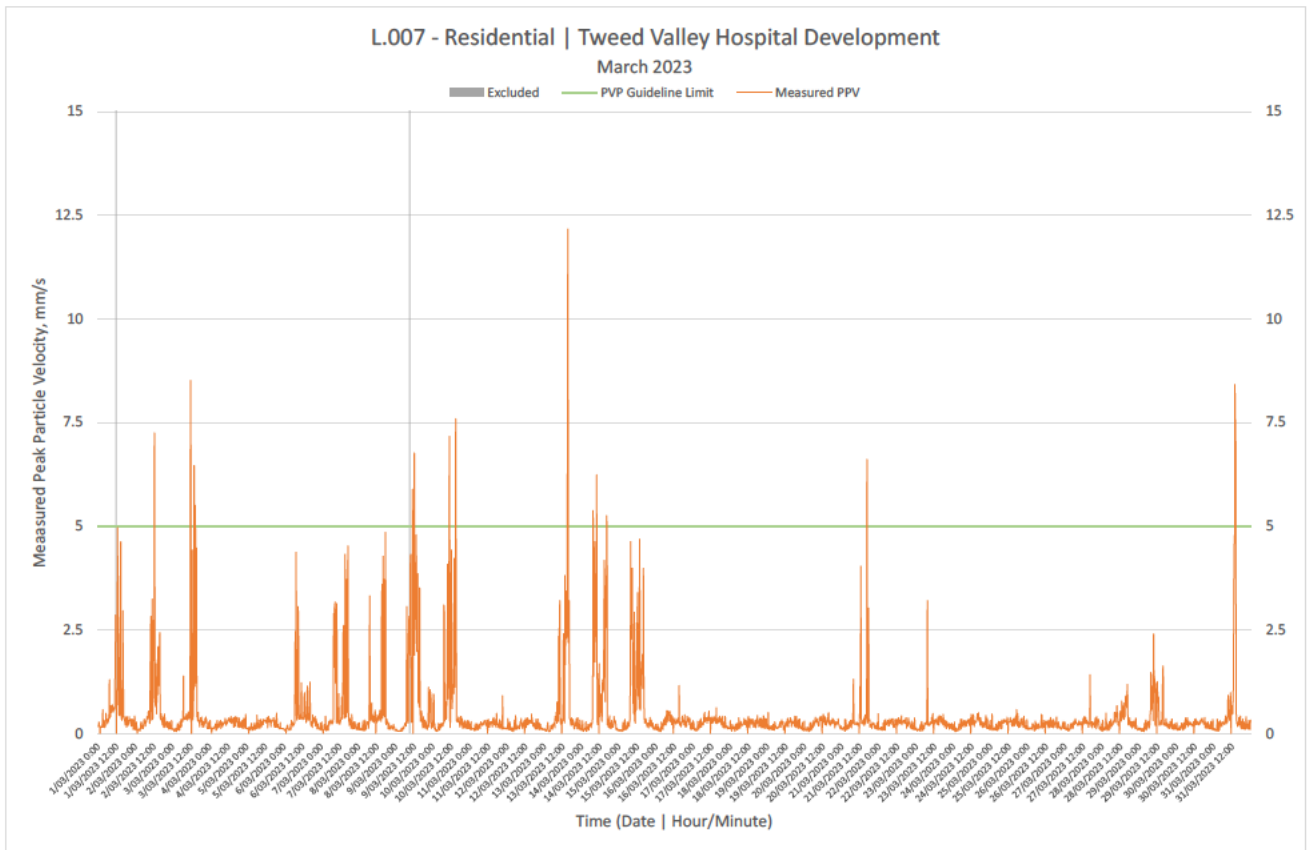


Figure 7 Velocity over time (Logger 007 – Residential)

Figure 8 illustrates the Frequency over Velocity for the data collected and analysed at Location L.007.

The increase in vibration energy outlined in both **Figure 7** and **Figure 8** is indicative of increased activity with the roadway including trenching works.

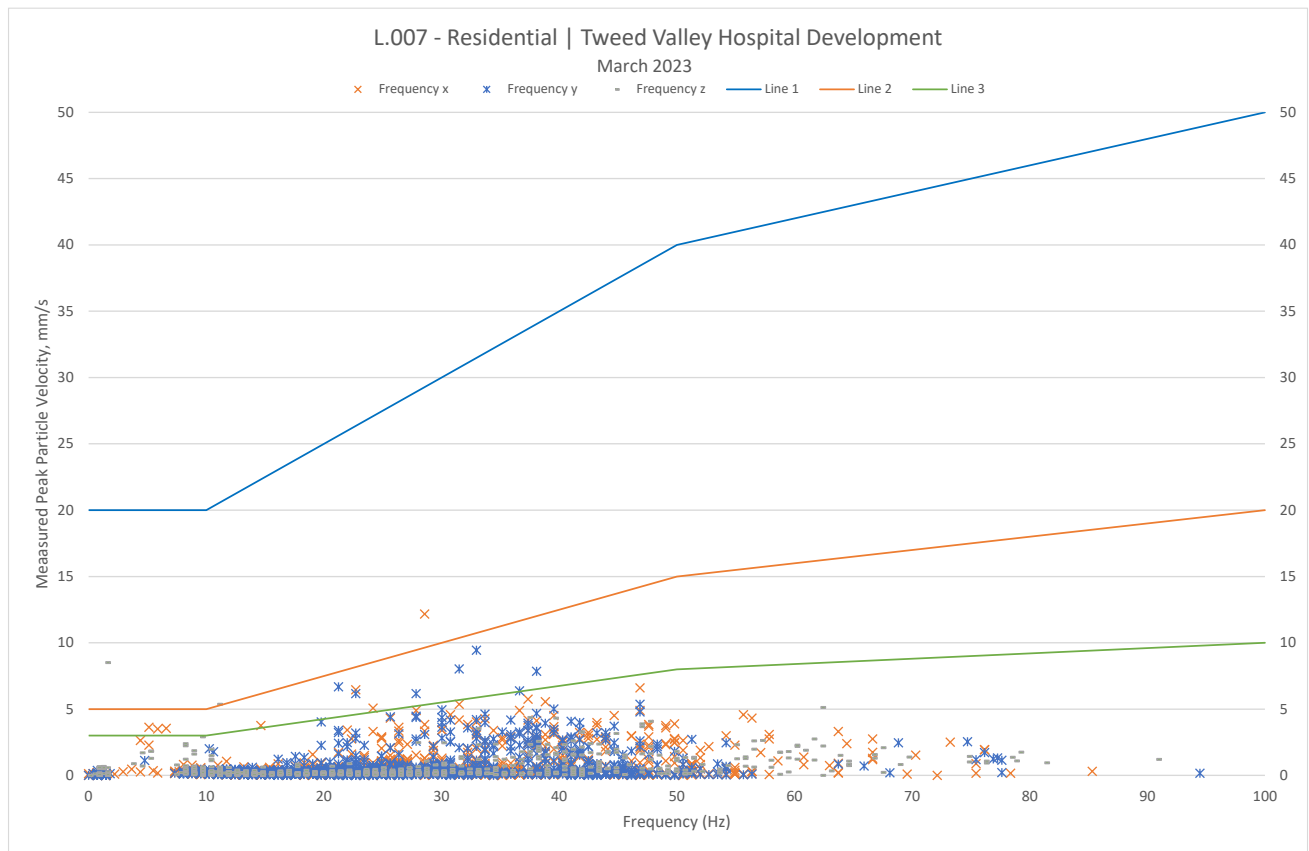


Figure 8 Frequency over Velocity (Logger 007 – Residential)

Most of the velocity levels exceeding 5 mm/s (the recommended velocity guideline for residential premises) is below the DIN4150 Line 2 guidelines. The guidelines and limitations outlined in **Section 2** are infrequently exceeded at the loggers location and no structural concern or impact is anticipated throughout the March period.

Where a structure may be considered dilapidated, low to mid frequencies may cause some minor cosmetic damage, however this is not anticipated based on analysis of the data.

3.2.2 Acceleration/VDV

During March 2023, road works along Cudgen Road were undertaken where large and heavy plant equipment operated along the anticipated alignment. Prior to these works, ADE undertook a Construction Noise and Vibration Impact Statement for the works. A screening assessment predicted a conservative estimated Vibration Dose Value (VDV) of $0.48 \text{ m/s}^{1.75}$ during a conservative scenario (at the facade of the receiver).

At Location L.005, six (6) days measured dosages exceeding the daytime goals were assessed. Four (4) days (March 10, 28, 29 and 31) VDV exceeded $0.8 \text{ m/s}^{1.75}$ indicating a high probability that an adverse comment may be received by a member of the community near the vibration sensors position.

At Location L.006, seven (7) days measured dosages exceeding the daytime goals were assessed. Two (2) days exceeded $0.8 \text{ m/s}^{1.75}$ and measurement data indicates that an adverse comment may have been likely.

At Location L.007, six (6) days measured dosages exceeding the daytime goals were assessed. Each of the six days measured between 0.4 and $0.8 \text{ m/s}^{1.75}$ indicating a mild probability of adverse comment.

Vibration data is attributed to road construction activities in close proximity to the sensors undertaken by CD Civil.

The results indicate that at the residence near this vibration logger, an adverse comment is possible as works along Cudgen Road proceed with heavy plant equipment.

Note that the vibration loggers are installed closer to the road carriageway than the facade of the nearest sensitive receiver and the results outlined here would be higher than what would be expected at the foundation of the residential building.

Figure 9 below presents VDV and weighted RMS Acceleration (α_{rms}) data measured at L.005.

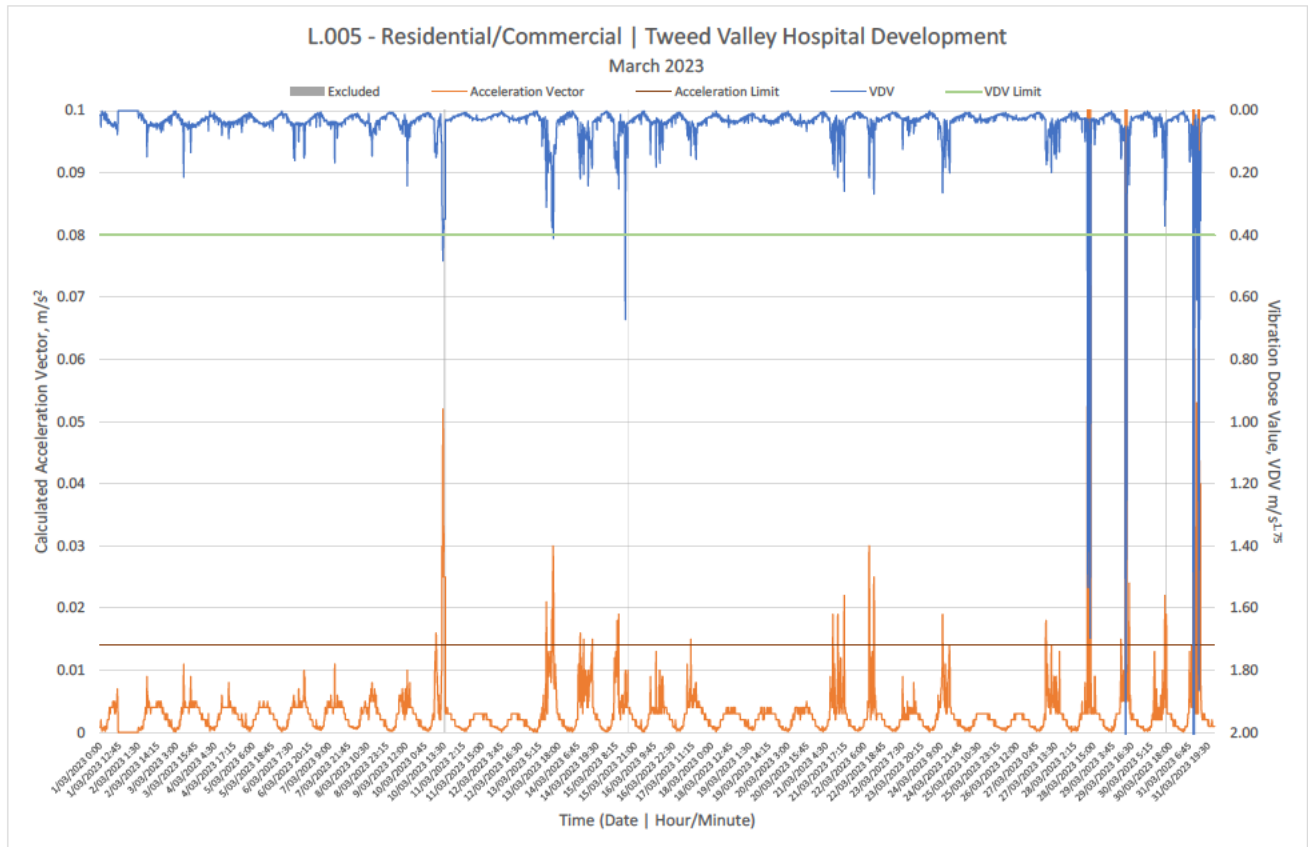


Figure 9 Acceleration and Vibration Dose Value over time (Logger 005)

The vibration impact at the commercial and residential premises is presented below in Figure 10. Generally, the measured data which is considered extraneous in nature (including ADE influence) has been removed from the data analysis and the graph.

The occupants at this location are less likely to have experienced any increase of perceptible vibration during the days where heavy plant equipment was in use, and the likelihood of adverse comment is not considered probable during these activities at this location during March.

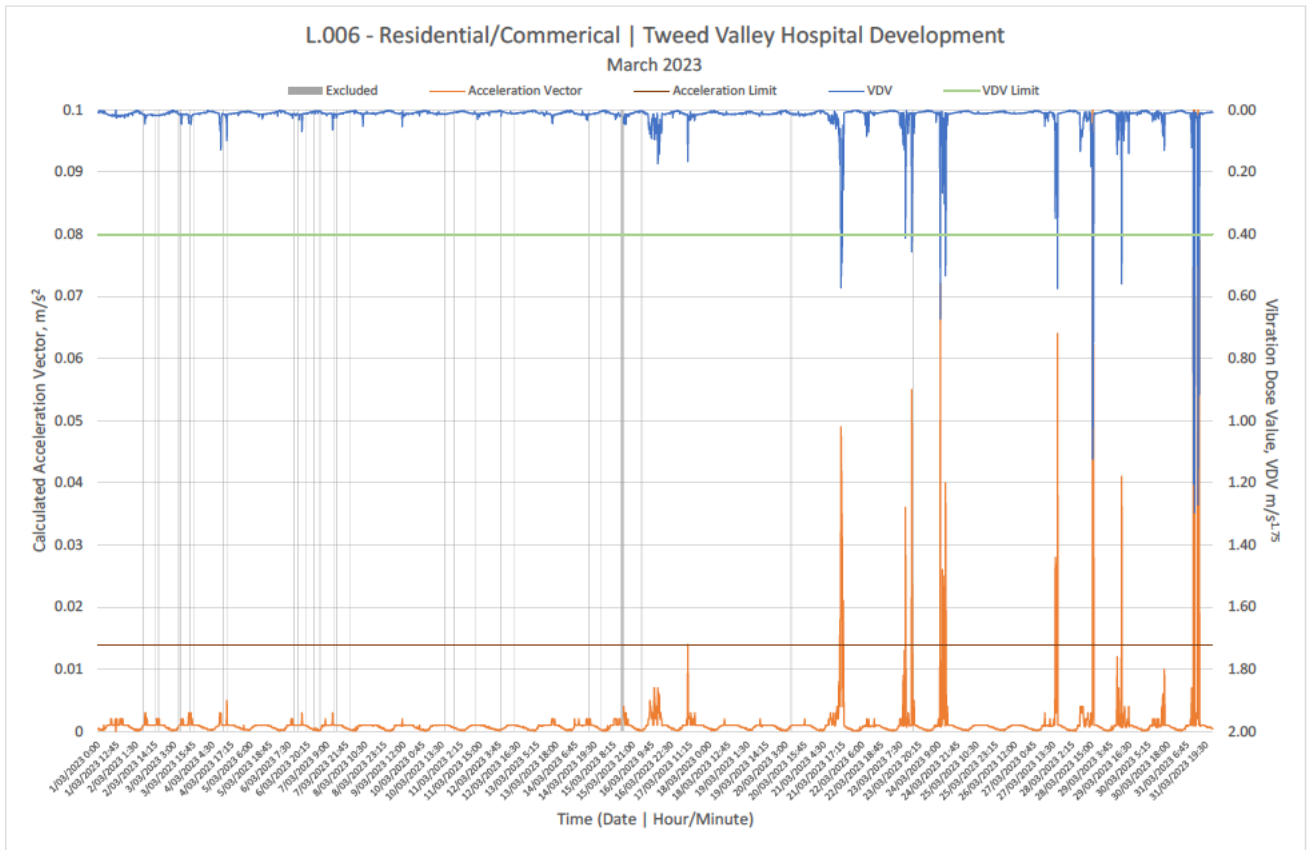


Figure 10 Acceleration and Vibration Dose Value over time (Logger 006 – Residential/Commercial)

Figure 11 which follows presents the increase in perceptible vibration at the southwestern residential receiver nominated as Location L.007.

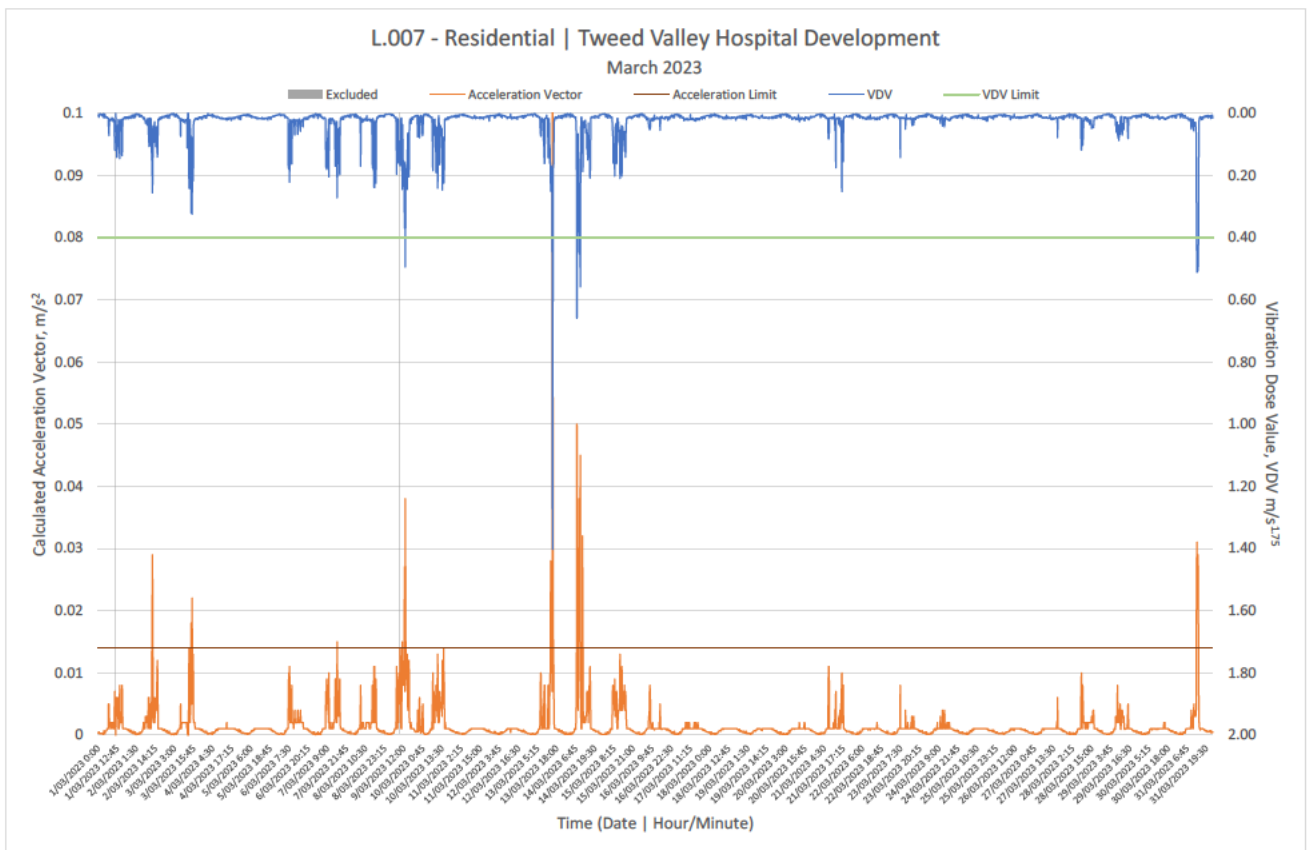


Figure 11 Acceleration and Vibration Dose Value over time (Logger 007 – Residential)

The occupants at this location (L.007) are likely to have experienced an increase of perceptible vibration during the days when heavy plant equipment was in use and the likelihood of adverse comment is probable.

3.3 Discussion

Vibration measurement and analysis of the data collected during March 2023 show a significant increase in vibration energy collected at each of the three sites. The Cudgen Road Upgrade Works where graders, asphalt machines, tracked excavators, large trucks, and multi-tyre/vibratory rollers are in active use in close proximity to each of the vibration loggers.

The impacts correlate with the data and known works of the site undertaken near the loggers, including:

- CD Civil excavating to full depth pavement on Cudgen Road. The heavy machinery in use includes 8T excavator, Grader, 9T Roller and Bobcat. The proximity to monitors is approximately 20 m
- Portable generators live throughout the day with the proximity to monitors being approximately 60 m
- Constant entrance/exit of trucks to site compound for spoil removal and material delivery through the main entrance. The trucks involved are semi-trailers, 6-wheelers etc. Proximity to monitors is approximately 30 m
- Installing stormwater drainage on Southern side of Cudgen Road. The plant included 8T excavator and plate compactors. The proximity to monitors is approximately 5 m
- Installation of the new watermain on the Southern side of Cudgen Road. The plant in used included a 8T excavator, 5T roller and plate compactors. Proximity to monitors is approximately 15 m.

Works operating at these distances would be anticipated to increase the degree of measured vibration at the location of ground sensors, which has the potential to impact the residential receivers near to the works and increase the likelihood of adverse comments by the community.

No comment or complaint was received during the March monitoring period. The implementation of all feasible and reasonable mitigation measures, and adherence to management practices is anticipated to reduce the vibration impact from the site and minimize any disturbance to occupants within sensitive premises'.

4 Conclusion

ADE Consulting Group Pty Ltd (ADE) was commissioned by Lendlease Group (Lendlease) to assess the levels of construction related vibration during the construction of the Tweed Valley Hospital Project and associated roadworks.

This report summarises vibration data collected at three locations, positioned along the south and southwest of Cudgen Road. At the time of preparing this report and the monitoring period in which it covers (March 2023), CD Civil are on site undertaking planned road work activities on Cudgen Road. These works include road profiling and grading, stormwater drain works, asphalt works and vibratory compaction.

The roadworks onsite have produced vibration levels anticipated, and as such a review of the data has been undertaken. The results are as follows:

Velocity

- Velocity values are exceeded at each location throughout the survey period
- Frequency analysis was conducted with some minor concerns pertaining to the frequency of velocity energy regarding cosmetic damage, however no structural concerns are present

Acceleration and Vibration Dose Values

- Human comfort is anticipated to be potentially intermittently impacted by residential receivers to the south and southwest of the project where acceleration and VDV measurement data exceeds the recommended values outlined in **Section 2**
- The perception of vibration is likely to be noticeable and cause some discomfort to residences occupying their premises during vibratory rolling/compaction works, or trenching activities
 - Other highly vibration intensive plant equipment may produce dosages which may exceed the guideline values and induce some community comment, notably during trenching works where tracked excavators are in frequent use
- The likelihood of adverse community comments has increased based on the dosages measured at the site at each location
- The measured dosages were during higher than normal extraneous data, conservative judgement places the data as works occurring on site near to the loggers ground sensor, although is not representative of the vibration which may be measurable or perceptible at the facade or foundation and is considered higher.

Appendix I – Glossary

1 Sound Pressure Level

Defined as:

$$L_p = 10 \log_{10} \left(\frac{p^2}{p_{ref}^2} \right) dB$$

In the above equation, p is the sound pressure fluctuation relative to atmospheric pressure, and p_{ref} is 20 microPascals (2×10^{-5} Pa), the approximate threshold of hearing.

Sound or noise is the sensation produced at the ear by small fluctuations in atmospheric pressure. Human ears are sensitive to changes to sound pressure over a wide range, from 20 microPascals to 60 Pascals, in lieu of using a linear scale to represent this range, a logarithmic scale is adopted to better handle

2 Sound Power Level

Sound power level cannot be directly measured using a microphone, it does not change with distance and is not influenced by atmospheric conditions. The sound power level refers to the total energy of the sound, and is reference to 1 Pico Watt.

3 Weighting and Loudness

The overall level of a sound is usually expressed as dB(A) and not dB. Weighting refers to the human ear's frequency response to sound. Typically, sound is measured with an A-weighted filter which reduces the significance of lower frequencies and very high frequencies, increasing the importance of mid-frequencies (500 Hz to 4 kHz), and being a good measure of the "loudness" of a sound.

A change of 1 to 2 dB(A) is difficult to detect, whilst a change of 3 to 5 dB(A) corresponds to a small but noticeable change. A 10 dB(A) change corresponds to a doubling or halving in apparent loudness.

4 Noise Metrics and Statistical Noise Levels

- i) L_{Aeq} - The time averaged A-weighted sound pressure level for the interval, as defined in AS1055.1. It is generally described as the equivalent continuous A-weighted sound pressure level that has the same mean square pressure level as a sound that varies over time. It can be considered as the average sound pressure level over the measurement period.
- ii) L_{Amin}/L_{Amax} - Minimum or Maximum A-weighted noise level detected during the measuring period. It refers to the minimum background noise detected or the maximum L_p measured.
- iii) L_{A90} - A-weighted noise level which is exceeded for 90% of the measuring period. It is usually used as

the descriptor for background noise level during the measurement period.

iv) L_{A1} - Noise level which is exceeded for 1% of the measurement period.

v) L_{A10} - Noise level which is exceeded for 10% of the measurement period. The L_{A10} is often referred to as the average *maximum* noise level.

5 Background Noise

The underlying level of noise present in the ambient noise, excluding the noise source which is under investigation, when extraneous noise is removed.

6 Ambient Noise

Ambient noise of an environment: the all-encompassing sound associated with that environment, being a composite of sounds from many sources.

7 Vibration

The mechanical oscillations occurring about an equilibrium point. The oscillations may be periodic such as the motion of a pendulum or random. Vibration is most commonly expressed in terms of displacement, velocity, acceleration and frequency, all of which are related

8 Displacement

The change in position of an object, is a vector quantity. (Stress indicator).

9 Velocity

The rate of change of displacement, is a vector quantity. (Fatigue indicator).

10 Acceleration

The rate of change of velocity, is a vector quantity. (Indicator of force).

11 Frequency

The number of times a periodic function or vibration occurs or repeats itself in a specified time, often 1 second – cycles per second. Frequency is measured in Hertz.

12 Hertz

The unit of frequency or pitch of a sound. One hertz equals one cycle per second.

13 Peak Particle Velocity (PPV)

The greatest instantaneous particle velocity during a given time interval if measurements are made in 3-axis. The resultant Peak Particle Velocity (PPV) is the vector sum i.e. the square root of the summed squares of the maximum velocities, regardless of when in the time history those occur.

14 Root Mean Square rms

The rms value of a set of numbers is the square root of the average of their squares. Best used when assessing building damage.

- 15 Vibration Dose Value VDV**
The Vibration Dose Value (VDV) is used for assessing intermittent vibration. A cumulative measurement of the vibration level received over an 8-hour or 16-hour period. Best used when the structure is occupied.
- 16 Peak**
The peak is the maximum amplitude during a measurement period.
- 17 Peak to Peak P-P**
The peak-to-peak (P-P) is the difference between the maximum positive and maximum negative amplitudes of a waveform.
- 18 Logarithmic Scale**
Comparing frequency with large amplitude differences be accomplished using a logarithmic scale. Critical vibration components usually occur at low amplitudes compared to the rotational frequency vibration. These components are not revealed on a linear amplitude scale because low amplitudes are compressed at the bottom of the scale, however a logarithmic scale shows prominent vibration components equally well at any amplitude.
- 19 Zero Crossing Frequency**
Determining the apparent dominate frequency of a given sample can be achieved by using the Zero Crossing Frequency.
- 20 Primary Waves P Waves**
Alternating compressions ('pushes') and dilations ('pulls') in the same direction as the wave is propagating. P waves are the first arriving energy, smaller and higher frequency than S waves.
- 21 Secondary Waves S Waves**
Alternating transverse motions perpendicular to the direction of propagation. Slower than P waves.
- 22 Rayleigh Waves R Waves**
Motion is both in the direction of propagation and perpendicular (in a vertical plane). R waves are also dispersive, and amplitudes decrease with depth.
- 23 Accelerometer**
A vibration sensor whose electrical output is directly proportional to the acceleration component of the vibration. The two most common accelerometer types are the traditional charge type and the IEPE, integrated electronic piezoelectric type with a built-in line-drive amplifier to enable the output signal to be transmitted over 'longer cable runs'.
- 24 Geophone**
Geophones measure velocity by means of a magnetic core surrounded by an electrical coil. When the surface vibrates, the geophone housing moves however the coil stays stationary, thus the movement of the magnet in the coil causes an electrical current which is calibrated to velocity of vibration.
- 25 Filter**
A device for separating components of a signal on the basis of their frequency. It allows components in one or more frequency bands to pass relatively unattenuated, and it attenuates components in other frequency bands. Modifies the frequency spectrum of a signal usually while it is in electrical form.
- 26 Short-term vibration**
Vibration which does not occur often enough to cause structural fatigue, and which does not produce resonance in the structure being evaluated.
- 27 Long-term vibration**
All types of vibration not covered by the definition of 'short-term vibration
- 28 Impulsive vibration**
Rapid build-up to a peak followed by a damped decay that may or may not involve several cycles of vibration. It can also consist of a sudden application of several cycles at approximately the same amplitude, providing that the duration is short (typically <2 seconds). Impulsive vibration (no more than 3 occurrences) in an assessment period is assessed on the basis of weighted rms acceleration, and peak particle velocity.
- 29 Continuous vibration**
Continuous vibration continues uninterrupted for a defined period (usually throughout daytime and/or night-time). This type of vibration is assessed on the basis of weighted rms acceleration.
- 30 Intermittent vibration**
Defined as interrupted periods of continuous (e.g., a drill) or repeated periods of impulsive vibration (e.g., a pile driver), or continuous vibration that varies significantly in magnitude. It may originate from impulse sources (e.g., pile drivers and forging presses) or repetitive sources (e.g. pavement breakers), or sources which operate intermittently, but which would produce Continuous vibration if operated continuously (for example, intermittent machinery, railway trains and traffic passing by). This type of vibration is assessed on the basis of vibration dose value.

Appendix II – Aerial Photograph

ADE Monitoring locations, site location (including CD Civil's Cudgen Road Upgrade works) are presented below.



Appendix III – References

Standards, policies, and guidelines used for the assessment of vibration are as follows:

- ADE Group Consulting Pty Ltd – Cudgen Road Upgrade Construction Noise and Vibration Impact Statement, Prepared for CD Civil, Version 1.0, 6 September 2022 (ADE Reference A103022.1044.00)
- Assessing Vibration: A Technical Guideline (February 2006), Department of Environment and Conservation (DEC)
- British Standard BS 7385-2:1993 Evaluation and measurement for vibration in buildings – Part 2: guide to damage Levels from ground-borne vibration
- British Standard BS 6472:2008 Guide to evaluation of human exposure to vibration in buildings – Part 1: vibration sources other than blasting
- Construction Noise and Vibration Strategy (April 2019) Published by Transport for New South Wales (TfNSW)
- Development Consent SSD-10353, Department of Planning, Industry and Environment – Tweed Valley Hospital Stage 2 – 12 July 2020 (approval)
- German Standard DIN 4150-1:2001 Structural vibration Part 1: Prediction vibration parameters
- German Standard DIN 4150-3:2016 Vibrations in buildings – Part 3: Effects on structures
- Tweed Valley Hospital Management Plan – Noise and Vibration, Revision 7.0, Lendlease Building Pty Ltd, 11 June 2019
- Tweed Valley Hospital – Noise and Vibration Impact Assessment for State Significant Development (SSD), SVM-2370, Revision: Issue 2, 17 October 2018 – Acoustic Studio

Appendix IV – Site Photographs



Photograph 1 Representative photograph of monitoring location 007 – Residential, as observed 13/03/2023



Photograph 2 Representative photograph of monitoring location 005 – Solar Industry, as observed 13/03/2023



Photograph 3 Representative photograph of monitoring location 006 – Mate and Matts, as observed 13/03/2023



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